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Associating Lattice Fluids near Hard and Interacting Walls

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Cubic lattice models of dimerizing and polymerizing fluids have been studied within Wertheim's Ornstein–Zernike (OZ) matrix formalism to assess the adsorption behavior of such fluids at impenetrable, interacting walls. The OZ matrix formalism is relatively easy-to-handle for these cubic lattice models, due to the absence of liquid-like packing effects. The calculated concentration profiles have been compared to NVT-Monte Carlo simulations. The simulation of the polymerizing fluid employed a biased cluster move, based on the configurational bias scheme of Siepmann and Frenkel. The dimerizing fluid profiles are in nearly quantitative agreement with the simulation results, even for a fully associated, i.e., dimeric fluid. This is in contrast with the polymerizing fluid profiles that show important deviations from the simulation results, especially near interacting walls. It is therefore concluded that better approximations are needed in solving Wertheim's OZ matrix for the polymerizing fluid.

1. Introduction

An associating fluid is characterized by short-ranged directional attractions between its particles. Studies of the bulk properties of associating fluids include the classical chemical theory of solutions in which the associative interactions are modeled as chemical reactions, lattice theories in which the free energy is minimized within the quasi-chemical approximation, computer simulation, and integral equation approaches (see ref 4 and references cited therein). The integral equation approaches attempt to accurately calculate the structural correlations between the fluid particles. The macroscopic thermodynamic properties can then be calculated from these correlations.5

In this paper Wertheim's Ornstein–Zernike (OZ) matrix integral equation for associating fluids with one9 and two9,10 directional attractive sites per particle is adapted to study the adsorption of associating cubic lattice fluids at an impenetrable interacting wall. As far as we are aware, it is the first application of Wertheim's OZ matrix integral equations to obtain the adsorption profiles of associating lattice fluids. Recently, work that uses a different integral equation approach for continuum adsorbing fluids has also been reported.10

We study the adsorption of lattice fluids, instead of the more realistic continuum fluids, because the OZ matrix formalism is very easy to handle in the case of lattice fluids. This is due to the absence of liquid-like ordering effects in such fluids. Also, it is very easy to introduce a flat wall into a cubic lattice fluid.11 Despite the simplicity of the cubic lattice model, it retains the main characteristic of an associating fluid: the formation of orientation-dependent bonds between the fluid particles. In the work reported here, we mainly consider the adsorption of fluids for which the associative interaction between the particles forms semipermanent (covalent) bonds that are not easily broken by the thermal motion of the particles. The fluids of particles with one (section 2) and two (section 3) directional attractive sites then serve to model the adsorption of molecular lattice fluids. Especially the doubly associating fluid is interesting to us, polymer chemists, for it models the adsorption of a polydisperse polymeric lattice fluid. Such polymeric lattice fluids are very commonly studied in polymer science12–16 and are technologically relevant, e.g., the composite and coatings industries.

The adsorption profiles that were obtained with the OZ matrix formalism have been compared to Monte Carlo simulations. For the fluid with one directional attractive force per particle, the profiles were simulated by the standard brute force method.17 The doubly associating fluid was simulated with a biased cluster move18 which combines the configurational bias scheme19 and a cluster move of Wu, Chandler, and Smit.20

The outline of the rest of this paper is as follows. In section 2 we delineate the equations for the calculation

(15) Theodoru, D. N. Macromolecules 1988, 21, 1400.
of the adsorption/depletion profiles of particles with one directional attractive force. Some attention is paid to the limit of infinitely strong attractions between the fluid particles. In this limit full association of the fluid particles into dimers occurs. In section 3 the formalism for fluids consisting of particles with two directional attractive forces is presented. For the case of strong associations between the particles, a polydisperse lattice fluid of polymeric chains near an impenetrable wall is formed.

The method that is used in sections 2 and 3 to introduce a wall into the fluid was developed by Henderson, Abraham and Barker to study the adsorption of a continuum fluid at a structureless surface. It was used by Yethiraj and Hall to obtain the static adsorption characteristics of a polymeric fluid at a hard wall within the RISM approach. Hall to obtain the static adsorption characteristics of a polymeric fluid at a hard wall within the RISM approach. The method consists of mixing a simple fluid particle into the associating fluid, after which this particle is "blown up" in two directions to form a flat wall. It is shown in sections 2 and 3 that it is particularly easy to employ this method on the cubic lattice. In section 4 we briefly outline the Monte Carlo simulation methods used for the singly and doubly associating lattice fluids. In section 5, the calculated adsorption profiles for the dimerizing and polymerizing fluids near hard and interacting walls are compared to the simulation data and the results are discussed. Conclusions are collected in section 6.

2. Adsorption of Particles with One Directional Attractive Force

In this section Wertheim's two-density formalism is adopted for the calculation of the adsorption profiles of a 3D cubic lattice fluid of singly associating particles at an impenetrable wall. The particles occupy exactly one lattice site and can bind into dimers due to an off-center associative particle–particle interaction. The walls are allowed to have a nonassociative interaction with the particles in the layer closest to the wall. The method used to introduce the wall into the fluid was developed to study the static adsorption behavior of continuum hard sphere fluids near an impenetrable structureless wall. For our case, its basic steps are as follows.

First, the Ornstein–Zernike matrix equation for a mixture of associating and simple (nonassociating) particles is written down. Then, the packing fraction of the simple fluid particles is reduced to zero. This assures that encounters of nonassociating simple particles are absent. After this, the simple particles are "blown up" along the m- and n-axis of the (l, m, n)-coordinate system by removing the m- and n-dependence of the correlations between the simple and associating particles. The average correlation between the wall and an associating particle can then directly be related to the concentration of the associating particles near the wall.

The potential model used to describe the interactions between the associating particles is

\[ u(1,2) = u_{R}(1,2) + u_{s,s_{1}}(1,2) \]  (1)

where (1,2) symbolically denotes the coordinates and orientations of particles 1 and 2. In eq 1, the repulsive part is only dependent on the distance (l, m, n) between particles 1 and 2:

\[ u_{R}(0,0,0) \rightarrow \infty \]

Note that \( u_{R}(l,m,n) \) regulates that the particles occupy exactly one lattice site. The attractive part of the potential \( u_{s,s_{1}}(1,2) \) is a function of the interparticle distance (l, m, n) and of the orientations \( \Omega_{1} \) and \( \Omega_{2} \) of the associatively bonded sites \( s_{1} \) and \( s_{2} \) on the particles:

\[ u_{s,s_{1}}(0,0,0,\Omega_{1},\Omega_{2}) = 0 \]

\[ u_{s,s_{2}}(l,m,n,\Omega_{1},\Omega_{2}) = u_{\text{attr}} \]

if \( \Omega_{1} = -\Omega_{2} \) and \( l^{2} + m^{2} + n^{2} = 1 \) and

\[ \text{sgn}(l + m + n)(l^{2} + 2m^{2} + 3n^{2}) = \Omega_{1} \]

where an attractive site can point in the directions +l (\( \Omega_{1} = 1 \)), -l (\( \Omega_{1} = -1 \)), +m (\( \Omega_{1} = +2 \)), -m (\( \Omega_{1} = -2 \)), +n (\( \Omega_{1} = +3 \)), and -n (\( \Omega_{1} = -3 \)). The conditions \( \Omega_{1} = -\Omega_{2} \) and \( l^{2} + m^{2} + n^{2} = 1 \) and \( \text{sgn}(l + m + n)(l^{2} + 2m^{2} + 3n^{2}) = \Omega_{1} \) assure that bond formation only occurs between nearest neighbor particles that have their attractive sites oriented toward each other (see Figure 1). The interactions that involve the nonassociating simple particles are considered further on.

In the two-density formalism, the packing fraction \( \eta \) of the associating particles, which is the fraction of the lattice volume filled with associating particles, is split into the fractions of particles that have \( \eta_{1} \) and have not \( \eta_{1} \) formed a bond with another associating particle

\[ \eta = \eta_{0} + \eta_{1} \]  (4)

The simple fluid particles do not have a directional attractive potential. Therefore, they are not involved in associative bonding and their packing fraction is not divided into parts as in eq 4. The Ornstein–Zernike matrix equation for a mixture of associating particles at packing fraction \( \eta \) and simple fluid particles at \( \eta_{M} \) is then given by

\[ H(1,2) = C(1,2) + \sum_{m,n} a H(3,2) \]  (5)

where the argument (1,2) denotes the dependence of \( H \) and \( C \) on the coordinates, i.e., position and orientation of the associating site, of particles 1 and 2. For the mixture of associating and simple particles, the matrix \( H(1,2) \) is given by

\[ H(1,2) = C(1,2) + \sum_{m,n} a H(3,2) \]  (5)
The (1,2) on the right hand side of eq 6 denotes that all elements of \( \mathbf{H} \) depend on (1,2). The matrix \( \mathbf{C}(1,2) \) is of the same form as \( \mathbf{H}(1,2) \). The \( h_{ij}(1,2) \) in eq 6 denote a part of the total correlation between two associating particles, the \( h_{ij}(1,2) \) denote a part of the total correlation between an associating and a simple particle, and \( h_{ij}(1,2) \) denotes the total correlation between two simple particles. The \( c_{ij}(1,2) \), \( c_{ij}(1,2) \), and \( c_{ij}(1,2) \) denote respectively the partial direct correlations between two associating particles, an associating and a simple particle, and two simple particles.\(^6\) The elements of \( \mathbf{H}(1,2) \) and \( \mathbf{C}(1,2) \) depend on the orientation \( \Omega \) of the attractive sites of each associating particle that is considered.

\[
h_{ij}(1,2) = h_{ij}(l,m,n,\Omega_1,\Omega_2)
\]

\[
h_{ij}(1,2) = h_{ij}(l,m,n,\Omega_2) = h_{ij}(l,m,n)
\]

We write \( h_{ij}(l,m,n,\Omega_2) = h_{ij}(l,m,n) \) because explicit orientational dependence only arises in the case of an interaction between two associating particles. If the third particle in eq 5 is a simple nonassociating particle, there is only a formal dependence on the orientation of this particle, and \( \Omega_1 \) can simply be replaced by the factor 6.

Before the closure equations necessary to calculate the adsorption profiles are introduced, we perform the matrix multiplications in eq 5 and take the limit \( \eta_M \to 0 \) to exclude encounters of simple fluid particles.

The result is nine equations distributed over four sets. The four sets are given by

\[
h_{ij}(1,2) = c_{ij}(1,2) + \frac{1}{6_{0,1,2,3}} \sum_{m,n} \left[ c_{0,1,3} \eta_0 h_{ij}(3,2) + c_{0,1,3} \eta_0 h_{ij}(3,2) \right]
\]

\[
h_{ij}(1,2) = c_{ij}(1,2) + \frac{1}{6_{0,1,2,3}} \sum_{m,n} \left[ c_{0,1,3} \eta_0 h_{ij}(3,2) + c_{0,1,3} \eta_0 h_{ij}(3,2) \right]
\]

\[
h_{ij}(1,2) = c_{ij}(1,2) + \frac{1}{6_{0,1,2,3}} \sum_{m,n} \left[ c_{0,1,3} \eta_0 h_{ij}(3,2) + c_{0,1,3} \eta_0 h_{ij}(3,2) \right]
\]

\[
h_{ij}(1,2) = c_{ij}(1,2) + \frac{1}{6_{0,1,2,3}} \sum_{m,n} \left[ c_{0,1,3} \eta_0 h_{ij}(3,2) + c_{0,1,3} \eta_0 h_{ij}(3,2) \right]
\]

with \( (i, j) \in \{0, 1, 2, 3\} \).

4. Fixation of \( (\eta, \eta_0) \) is therefore analogous to the setting of \( \eta \) and the strength of the associative interaction, \( u_{at} \).

The last set in eq 9 consists of a single equation for the total correlation \( h_{ij}(1,2) \) between two simple particles. It is of no concern to us due to the limit \( \eta_M \to 0 \) that we have taken. Further, we only need to consider one of the two sets, the second or third in eq 9, for the wall-associating particle correlations \( h_{ij}(1,2) \). Both these sets can be employed, but we choose to use the third. This set, which consists of two equations, can be written in an orientation independent form without approximation, because we are considering parts of the orientation independent distribution (see eq 8) of an associating and a simple particle. Therefore, we can write

\[
h_{ij}(l,m,n) = c_{ij}(l,m,n) + \sum_{m,n'} (\eta_0 h_{ij}(l,m',n') + \eta_0 h_{ij}(l,m',n')) c_{ij}(l'-m'-n',m'-m')
\]

\[
= \eta_0 h_{ij}(l,m',n') c_{ij}(l'-m'-n',m'-m')
\]

\[
h_{ij}(l,m,n) = \eta_0 h_{ij}(l,m',n') c_{ij}(l'-m'-n',m'-m')
\]

Equation 11 is the central result of this section. Note that the \( h_{ij}(l,m,n) \), which are the parts of the correlation between two associating particles, are still dependent on three coordinates.

The \( h_{ij}(l) \), that are found from eq 11 upon combination with an appropriate closure equation, are the partial wall-associating particle correlations that can be used to construct the concentration profile of the associating fluid at the wall.

We have complemented eq 11 with a Percus–Yevick type closure relation, given by

\[
y_{ij}(l) = g_{ij}(l) - c_{ij}(l)
\]

and the exact relations

\[
g_{ij}(l) = e^{-\delta_{ij}w(l)}
\]

in which \( w(l) \) is the symmetric \( (w(\pm l) = w(-l)) \) wall-associating particle potential. It is given by

\[
u_{w}(0) = +\infty
\]

\[
u_{w}(\pm l) = u_{w}
\]

Equation 15 (and eqs 12 and 13) deals with only one associating particle, which explains the single index.
Equations 11–15 form a complete set of equations that can be solved for the \( h_i(l) \), if we have obtained \( h_{ij}(l,m,n) \) from the first set in eq 9 with the methods outlined in ref 23. The solution method for obtaining the \( h_i(l) \) is outlined in the Appendix. Once the \( h_i(l) \) are known, the partial wall–fluid distributions \( g(l) \) are found from eq 15. The concentration profile can then be constructed from

\[
\eta g(l) = \eta g_0(l) + \eta_0 g_0(l)
\]

From the concentration profile \( \eta g(l) \), an excess adsorbed amount \( \Gamma \) is defined by

\[
\Gamma(\eta) = \sum_{l=1}^{l_{\text{bulk}}} \eta g(l) - 1
\]

where \( g(l) - 1 \) denotes the deviation of the associating fluid distribution at the wall from the bulk value 1. The \( l_{\text{bulk}} \) should be chosen large enough for the summation to reach into the bulk of the adsorbing fluid. An adsorption isotherm is constructed by plotting \( \Gamma(\eta) \) versus \( \eta \).

Note that the theory outlined in this section does not provide the correlations between the associating particles in the interfacial layers. It only considers wall–fluid correlations. The method outlined in this section can also be used to study the adsorption of associating particles on an attracting “rod” if only one coordinate is removed in going from eq 10 to eq 11. Results for the static adsorption behavior of the singly associating fluid near an attracting wall are presented in section 5.

### 3. Adsorption of a Polymerizing Cubic Lattice Fluid

In this section the three-density formalism\(^8,9\) is adapted to calculate the concentration profiles of a cubic lattice fluid consisting of particles with two directional attractive forces at an impenetrable wall. The wall is again allowed to have a nonspecific nearest neighbor interaction with the particles that occupy one lattice site each. The method itself is completely analogous to the method described in the previous section. If the attractions between the doubly associating particles are relatively strong, chain molecules will be formed. The density profiles are therefore the result of the adsorption of a polydisperse polymeric lattice fluid at an impenetrable wall.

The potential model that is used involves a summation over the two attractive sites of each particle:\(^8\)

\[
u(1,2) = u_R(1,2) + \sum_{s_1=1}^{2} \sum_{s_2=1}^{2} u_{s_1,s_2}(1,2)
\]

The potentials \( u_R \) and \( u_{s_1,s_2} \) are defined by eqs 2 and 3, respectively. We have chosen the sites on a particle to be indistinguishable. Kalyuzhnyi and Stell\(^{24}\) have generalized Wertheim's approach\(^{18,19}\) to such systems, and here we rely on their graphical analysis.

The OZ matrix equation for a system of simple particles at packing fraction \( \eta_M \) and doubly associating particles at packing fraction \( \eta \) is still given by eq 5 with the modified matrices

\[
\mathbf{H}(1,2) = \begin{bmatrix}
ono & h_{00} & h_{01} & h_{02} & h_0 \\
h_{10} & h_{11} & h_{12} & h_1 \\
h_{20} & h_{21} & h_{22} & h_2 \\
h_0 & h_1 & h_2 & h
\end{bmatrix}
\]

and

\[
\sigma = \begin{bmatrix}
s_2 & s_1 & s_0 & 0 \\
s_2 & 0 & 0 & 0 \\
s_0 & 0 & 0 & 0 \\
0 & 0 & 0 & \eta_M
\end{bmatrix}
\]

in which

\[
\sigma_i = \sum_{j=0}^{n} \eta_j
\]

with \( \{i, j\} \in \{0, 1, 2\} \) and \( \eta = \eta_0 + \eta_1 + \eta_2 = \sigma_2 \). The \( \eta_j \) in eq 21 denote the packing fractions of the associating particles that have formed \( j \in \{0, 1, 2\} \) specific bonds. The matrix for \( \mathbf{C}(1,2) \) is of the same form as the \( \mathbf{H}(1,2) \) matrix. The \( h_{ij}(1,2) \) in eq 19 denote parts of the total two-particle correlation between two associating particles; the \( h(1,2) \) concern an associating and a simple particle, and \( h(1,2) \) is the total correlation between two simple particles.

Matrix multiplication of eq 5 and taking the limit \( \eta_M \to 0 \) results in sixteen equations distributed over four sets:

\[
h_{ij}(1,2) = c_{ij}(1,2) + \frac{1}{6} \sum_{rs} [c_{0(1,3)} c_{2r} h_{0}(3,2) + c_{0(1,3)} c_{1r} h_{0}(3,2) + c_{0(1,3)} c_{0r} h_{0}(3,2)] +
\]

\[
h_{11}(1,2) = c_{11}(1,2) + \frac{1}{6} \sum_{rs} [c_{0(1,3)} c_{1r} h_{0}(3,2) + c_{0(1,3)} c_{0r} h_{0}(3,2) + c_{0(1,3)} c_{0r} h_{0}(3,2)] +
\]

\[
h_{12}(1,2) = c_{12}(1,2) + \frac{1}{6} \sum_{rs} [c_{0(1,3)} c_{1r} h_{0}(3,2) + c_{0(1,3)} c_{0r} h_{0}(3,2) + c_{0(1,3)} c_{0r} h_{0}(3,2)] +
\]

\[
h_{13}(1,2) = c_{13}(1,2) + \frac{1}{6} \sum_{rs} [c_{0(1,3)} c_{1r} h_{0}(3,2) + c_{0(1,3)} c_{0r} h_{0}(3,2) + c_{0(1,3)} c_{0r} h_{0}(3,2)] +
\]

The first set in eq 22 comprises nine equations, and the second and third set each contain three equations. The fourth set contains only one equation. The set for the \( h_{ij}(1,2) \) in eq 22 contains the equations that determine the parts of the total two-particle correlations in the bulk associating fluid. It was solved in ref 18 by combining it with PY-type closures and mass balance equations. In obtaining the \( h_{ij}(l,m,n) \) of the bulk fluid, it was necessary\(^{18,25}\) to assume the independence of the two interaction sites on the associating fluid particles and to preaverage the site–site potential \( u_{s_1,s_2} \) over the orientations of the


sites. The preaveraging is given by

\[ f_A(l, m, n) = \frac{1}{36} \sum_{\alpha_1, \alpha_2} (e^{-\phi_{\alpha_1\alpha_2}(l, m, n, \alpha_1, \alpha_2)} - 1) \]  

which results in

\[ f_A(l, m, n) = \frac{1}{36}(a - 1) \quad \text{if } l_2 + m_2 + n_2 = 1 \]
\[ f_A(l, m, n) = 0 \quad \text{otherwise} \]  

(24)

with \( a = e^{-\phi_{\alpha_0\alpha_0}} \). The \( f_A \), which is the attractive part of the Mayer function, appears in the closure and mass balance equations of the bulk fluid. The \( h(l, m, n) \) of the bulk fluid are needed in this section as an input for the calculation of the adsorption profiles. In this section, we therefore also assume the independence of interaction sites on an associating particle and employ the preaveraging of eq 24. The last set of eq 22 is a single equation for the total correlation of two simple particles. It is of no importance that the box that was bounded by impenetrable walls on both sides along the \( l \)-axis. The box had periodic boundaries in the \( m \)- and \( n \)-directions. Layers were defined as \( m \)-planes parallel to the impenetrable walls. Particles in the layer closest to the wall experience a wall–particle interaction. Systems with zero or an attractive wall–particle energy \( u_W \) were considered. The concentration profiles were determined by counting the numbers of particles in each layer.

Equilibration was assured by monitoring the internal energy, \( E \), of the fluid in the box and by checking that the obtained concentration profiles were symmetric along the \( l \)-axis. A blocking method was used to calculate the standard deviations of the monitored averages and to assure that the simulation recipe is able to produce uncorrelated data. Thus far, we have only determined the concentration profiles from the simulations, but in the case of the polydisperse chain fluid it might also be interesting to study ordering, reorientation, and chain length segregation effects that are induced by the impenetrable wall.

Both types of fluids that we have considered were tested at two box filling fractions: \( \eta' = 0.5 \) with 1000 particles in a \( 20 \times 10 \times 10 \) mm box and \( \eta' = 0.3 \) with 1536 particles in a \( 20 \times 16 \times 16 \) mm box (the overall box filling fractions are denoted as \( \eta' \) to distinguish them from the packing fraction \( \eta \) of the bulk region). The walls were non-interacting or had a favorable attractive energy of \( u_W = -0.25k_B T \) or \( u_W = -0.5k_B T \) with the particles in the layers closest to the wall. Different runs were performed with associating particle–particle interactions varying from \( u_W = -1.0k_B T \) to \( u_W = -7.0k_B T \) (in steps of \(-0.5k_B T \) or \(-1.0k_B T \)).

The simulation recipe that was used is different for both fluid types. For the simulation of the singly associating fluid, we have used a combination of brute force moves and moves in which a particle was taken from a dimer and bonded to a free nonbonded monomer. The latter move is included in the recipe because there is generally no energy difference associated with it, leading to automatic acceptance and enhanced equilibration. Only when a particle is moved from or to a layer next to the wall do we have to take the wall–associating particle interaction energy into account in the acceptance criterion of this move. It samples the distribution of the particles over the lattice but does not sample the number of particles bonded into a dimer. Therefore, we also need to include a sufficient amount of brute force moves in the recipe.

A recipe was employed in which 70% brute force and 30% other moves were attempted. The average energy in the box and the concentration profiles were tested to be independent of the exact constitution of the recipe.

The simulation recipe of the polymerizing fluid was used previously to obtain the structural properties of the bulk region of the fluid. It includes brute force moves (10%), bond flips (10%), double bond flips (15%), generalized reptation moves (15%), and biased cluster moves (50%). I indicated between the parentheses are the percentage of attempts for the type of move. The polymerizing particles interact via the model potential of 2, 3, and 18. It is forbidden for the two sites on a particle to point in the same direction, and the chains that are formed thus show the full excluded volume. Note that this is not the case in the theory of section 3, because in solving the OZ matrix one has to assume an independence of the orientations of the attractive sites on the particles, as outlined above eq 24.

All moves used in the recipe were discussed in detail in ref 18. The only difference is that in this work the

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wall—particle interaction needs to be accounted for in the acceptance criterion of the moves. The brute force move consists of randomly choosing a new particle position and two orientations for the attractive sites of a randomly chosen particle. Acceptance of the move is determined by the conventional Metropolis acceptance criterion. The bond flip attempts to change the orientation of one of the attractive sites of a particle without moving the particle. It is meant to sample the creation/destruction of chain ends in the polymerized fluid. The third move, the double bond flip, samples the chain length distribution by imitating a metathesis reaction (see Figure 2).

This move was introduced by Olaj and Lantschbauer and by Mansfield in the simulation of a polydisperse polymeric lattice fluid at full packing. The fourth move, the generalized reptation move, consists of randomly choosing two chain ends and flipping the end segment of one chain to the other chain. This move helps to sample the particle distribution on the lattice. Acceptance of the bond flips and the generalized reptation moves is again governed by the Metropolis acceptance criterion. Note that there is generally no energy difference associated with the double bond flips and generalized reptation moves. The last move, the biased cluster move, was first presented in ref 18. It consists of two parts. The first part, the cluster part, is concerned with the selection of a part of a polymeric chain molecule: the cluster. The cluster may consist of many particles; therefore, in moving the cluster we need to alter the form of the cluster in such a way that it fits into the voids present between the other particles in the box. This is what the second part, the configurational bias scheme, is concerned with. The bias that is introduced by adjusting the form of the cluster is corrected for in the acceptance criterion. The final scheme, the bias cluster scheme, has the additional feature that it samples chain lengths. This property is most welcome in our study of polymerizing fluids in which the chains do not have fixed lengths. In ref 18, it was shown for a polymerizing bulk fluid that the bias cluster move is more efficient than simple brute force moves. Note that, in the simulation of the polymerizing fluid adsorption profiles, we need to include the wall—fluid interaction in the Rosenbluth factors.

All simulations were performed in nonparallel runs on a 14 MIPS R8000 processor Silicon Graphics Power challenge XL with an IRIX 6.0 operating system. Simulations for the dimerizing fluid took up to 2 CPU hours for the strongly interacting fluids ($u_{\text{attr}} = -7.0 k_B T$). The polymerizing fluid simulations took up to 10 CPU hours for $u_{\text{attr}} = -7.0 k_B T$ and 5 hours for $u_{\text{attr}} = -3.0 k_B T$. The results are available on request via e-mail at tgpken@urctue.nl.

5. Results and Discussion

5.1. Dimerizing Fluid. In Figure 3 some concentration profiles of the singly associating lattice fluid are presented. Walls are located at layer l = 0 and layer l = 21. Symmetric profiles along the l-axis are obtained, but only layers 1–8 are shown. Three wall—fluid nearest neighbor interactions were considered in Figure 3: $u_{\text{wall}} = 0.0 k_B T$ (■), $u_{\text{wall}} = -0.5 k_B T$ (■), and $u_{\text{wall}} = -0.0 k_B T$ (●). The simulations were performed for a box filling fraction $\eta' = 0.25$ and $u_{\text{attr}} = -7.0 k_B T$. From the simulations we have found $\eta_0$ to be 0.2852 and 0.03177 (●), 0.2939 and 0.0320 (■), and 0.3019 and 0.0320 (●). With these values of $\eta$ and $\eta_0$ we have calculated the lines in the figure according to the OZ formalism of section 2.
Note that the most appropriate comparison between the theory and the simulations would have been at fixed \( \eta \) and \( u_{\text{attr}} \) because it is these two quantities that determine \( \eta_0 \). It was found previously\(^{23}\) that it is fully justified to make the comparison at fixed \( \eta \) and \( \eta_0 \) if \( |u_{\text{attr}}| > 3k_B T \).

Comparisons between the theory and simulations for other bulk packing fractions and degrees of association have been made and show the same excellent agreement. Therefore, we have not depicted the full concentration profiles for such situations. An overview of the adsorption behavior at box filling fraction \( \eta > 0.5 \) and \( u_{\text{attr}} = 0.0 k_B T \) (\( \bullet \)), \( u_{\text{attr}} = -0.25 k_B T \) (\( \blacksquare \)), and \( u_{\text{attr}} = -0.5 \) (\( \triangle \)) is given in Figure 4, where the amount of adsorbed material in the layer closest to the wall is plotted versus the associative interaction strength \( u_{\text{attr}} \). The comparison between simulation and theory is for the \( \eta \) and \( \eta_0 \) observed from the simulations. Therefore, the (very small \( \approx \pm 0.001 \)) numerical inaccuracies in the \( \eta \) and \( \eta_0 \) obtained from the simulations also show up in the calculated curves, which explains why the curves in Figure 4 are not completely smooth.

Several interesting aspects can be observed from Figure 4. First of all it is seen that the agreement between theory and simulation is excellent for the \( u_{\text{attr}} \) values that have been considered. Second, comparing the \( g(1) \) values of Figure 3 (\( g(1) = 1.460 \)) and Figure 4 (\( g(1) = 1.2715 \)) for \( u_{\text{attr}} = -0.5 k_B T \) and \( u_{\text{attr}} = -7.0 k_B T \) shows that in the cases of the higher bulk packing fraction \( \eta = 0.2852 \) in Figure 3 and \( \eta = 0.4854 \) in Figure 4 the tendency of the fluid to accumulate at the wall is less strong: there is a diminishing of the wall–particle correlations for higher bulk packing fractions, simply because the packing fraction at the wall can never exceed unity.

It is also seen in Figure 4 that \( g(1) \) is almost fully determined by \( u_{\text{attr}} \) and that \( u_{\text{attr}} \) is only of minor influence. This means that the favorable energetic wall–particle interaction is more important than the entropic depletion, which occurs due to ordering of the dimeric molecules at the wall. It is shown in the next subsection that the effect of \( u_{\text{attr}} \) on the concentration of the fluid near the wall is much more influential for polymerizing fluids, because in that case \( u_{\text{attr}} \) has a large effect on the size of the molecules that are formed.

A last aspect of Figure 4 is observed by looking at the dependency of \( g(1) \) on \( u_{\text{attr}} \) for the three lines in the figure. The lower curve for which \( u_{\text{attr}} = 0 \) shows a decrease of \( g(1) \) for higher \( |u_{\text{attr}}| \): a somewhat deeper depletion hole is observed for a more highly dimerized fluid. Thus, the entropic depletion, which is the only determining factor near a non-interacting wall, is more important for more highly dimerized systems. For the upper curve, for which \( u_{\text{attr}} = -0.5 k_B T \), the situation is reversed. Not only do the fluid particles tend to accumulate (\( g(1) > 1 \)) at the wall, the accumulation also increases for a stronger associative interaction \( u_{\text{attr}} \): the dimers have a stronger tendency to accumulate at the wall than the nonbonded particles, in spite of the entropic restrictions that the wall imposes on the dimers. This is because the gain in energy that accompanies the adsorption of a dimer is larger than the entropy loss. For \( u_{\text{attr}} = -0.25 k_B T \) this is not the case. Although an accumulation of particles at the wall is observed from Figure 4 for \( u_{\text{attr}} = -0.25 k_B T \), we see a slight decrease of \( g(1) \) for a strongly associating fluid: the wall–particle interaction is not strong enough to counterbalance the entropic restriction the wall imposes on the adsorbing dimers. A decrease of \( g(1) \) is therefore observed for increasing \( u_{\text{attr}} \).

In Figure 5, the adsorption profile in the limit of infinitely strong association, \( u_{\text{attr}} \to -\infty \), for which a fully dimerized lattice fluid is obtained, is drawn (full line). The symbols in Figure 5 denote points obtained with a previously outlined \( N_pT \) simulation method. The simulation method does not attempt to break bonds between particles. This would lead to immediate rejection of the move for the fully associated fluid (\( u_{\text{attr}} \to -\infty \)). Therefore, we have only sampled the distribution of the dimers over the lattice by moving them in a reptation-like fashion through the simulation box. Figure 5 clearly demonstrates the accuracy of the associating fluid theory for \( u_{\text{attr}} \to -\infty \). Identical results have been found at other packing fractions (up to \( \eta = 0.7 \)).

We conclude from the results presented in this section that the general performance of Wertheim's formalism\(^{6,7}\) is excellent when applied to study the adsorption profiles of singly associating cubic lattice fluids at hard and interacting impenetrable walls.

5.2. Polymerizing Fluid. In Figure 6, some adsorption profiles of a polymerizing fluid with \( u_{\text{attr}} = -7.0 k_B T \) at overall box filling fraction \( \eta = 0.3 \) are depicted. The symbols indicate the simulation results. The lines depict the results obtained from the theory. The bulk packing fractions that were monitored are summarized in Table 1, together with the number average chain length \( L_n \) and

\begin{align*}
\text{(31) Nies, E.; Cifra, P. Macromolecules 1994, 27, 6033.} \\
\end{align*}
we also use eq 27 to analyze the simulation results; lines correspond to the solution of the equations of section 3 with $u_w = 0.0 k_B T$ (dashed line, $\bullet$) and $u_w = -0.25 k_B T$ (full line, $\blacksquare$). In both cases, $u_{attr} = -0.70 k_B T$ and $\eta' = 0.3$.

**Table 1. Overview of Number Average Chain Lengths and Widths of Distribution**

<table>
<thead>
<tr>
<th>Symbols/lines</th>
<th>$\eta$</th>
<th>$L_N$</th>
<th>$L_W/L_N$</th>
</tr>
</thead>
<tbody>
<tr>
<td>Figure 6</td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>$\bullet$</td>
<td>0.3156</td>
<td>11.7</td>
<td>1.92</td>
</tr>
<tr>
<td>$\blacksquare$</td>
<td>0.2959</td>
<td>11.6</td>
<td>1.91</td>
</tr>
<tr>
<td>- - -</td>
<td>0.3156</td>
<td>12.021</td>
<td>1.917</td>
</tr>
<tr>
<td>- - -</td>
<td>0.2959</td>
<td>11.605</td>
<td>1.938</td>
</tr>
<tr>
<td>ref 18 bulk values</td>
<td>0.3015</td>
<td>11.8</td>
<td>1.92</td>
</tr>
<tr>
<td>Figure 7</td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>$\bullet$</td>
<td>0.5113</td>
<td>15.6</td>
<td>1.94</td>
</tr>
<tr>
<td>$\blacksquare$</td>
<td>0.4956</td>
<td>15.5</td>
<td>1.94</td>
</tr>
<tr>
<td>- - -</td>
<td>0.5113</td>
<td>15.764</td>
<td>1.937</td>
</tr>
<tr>
<td>- - -</td>
<td>0.4956</td>
<td>15.483</td>
<td>1.935</td>
</tr>
<tr>
<td>ref 18 bulk values</td>
<td>0.5</td>
<td>15.5</td>
<td>1.94</td>
</tr>
</tbody>
</table>

$^a$ In all cases: $u_{attr} = -7.0 k_B T$.

width of the chain length distribution $L_W/L_N$. These were obtained from the simulations with Flory’s formulas:

$$L_N = \frac{1}{1 - p}$$

$$L_W/L_N = 1 + p$$

(27)

with the extent of reaction $p$ defined by

$$p = \frac{\eta'_1 + 2\eta'_2}{2\eta'}$$

(28)

in which $\eta'_i$ is the average packing fraction in the simulation box and $\eta'_1$ are the whole box average packing fractions of particles with $i$ bonds. In eq 27, the formation of rings is neglected.

This results in an overestimation of the actual chain length of up to 10% for the systems considered here. Although it is possible to obtain the actual $L_N$ and $L_W/L_N$ from the simulations by monitoring the full chain length distribution, it is not possible to obtain the full chain length distribution from the theory of section 3. Therefore, to compare identical quantities, we use eq 27 to analyze the simulation results.

The $L_N$ and $L_W/L_N$ monitored from the simulations are a function of the layer number, but thus far we have not monitored the $L_N$ for each layer separately. Therefore, we have only calculated whole box averages, although it is expected that there is a preference close to the wall for shorter chains when compared to longer chains: the entropic restrictions that the wall imposes on the molecules (restrictions on molecule conformation and surface-induced ordering of the molecules) are smaller for shorter chains. Monitoring of the fractions of free, singly bonded, and doubly bonded particles for each layer separately would allow us to study this surface-induced segregation effect. In Figure 6, we are dealing with relatively short chains, $L_N \approx 12$, for which we expect the effect to be small. Although we have no direct proof of this, we can nevertheless see from Table 1, by comparing the whole box averages obtained in this work with the averages obtained previously for the bulk region, that the surface segregation is not strong enough to cause strong deviations of the overall $20 \times 10 \times 10$ box values of $L_N$ and $L_W/L_N$ from the values for the bulk region. This does not imply, however, that the influence of the walls is unimportant in the layers close to the wall.

Figure 7 is identical to Figure 6 but for $\eta' = 0.5$. Bulk packing fractions, number average chain lengths, and widths of the distribution are again given in Table 1. The bulk values taken from ref 18 are also reported in Table 1. Comparison with the bulk values again shows that the walls do not have a large influence on the overall averages obtained from the box.

The agreement between the calculated and simulated adsorption profiles in Figures 6 and 7 is not overall good. In the case of non-interacting walls (dashed lines) the theory seems to be qualitatively correct. It does predict a depletion hole, although the hole is not deep enough when compared to the simulation results. The origin of the depletion hole is the entropic penalty that the wall imposes on the fluid. It is not compensated by an attractive wall–fluid interaction, and therefore, a depletion of the fluid near the wall is observed.

For the interacting walls, $u_w = -0.25 k_B T$ (full lines), both the theory and the simulations show an accumulation of particles at the wall. This accumulation is due to an energetically favorable wall–fluid interaction $u_{w}$ that compensates the entropic depletion. For $u_w = -0.25 k_B T$ (full curve) in Figure 6, the theory and the simulations both show an accumulation of particles near the wall, but we find that the theory underestimates the total amount of adsorbed material, especially in the second layer from the wall. For $u_w = -0.25 k_B T$ (full curve) in Figure 7, the theory predicts an almost flat profile: the entropic depletion and energetic accumulation are nearly balanced in the theory. The simulations, on the other hand, show a net accumulation of particles near the wall.

In both figures, the simulations for $u_w = -0.25 k_B T$ (full) show the formation of a block profile near the wall. Especially in Figure 6, the two layers closest to the wall are rather densely packed, while there is a sharp decrease

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of the packing fraction in going from the second to the third layer. In Figure 7, this effect is also observed, although it is less pronounced. The block formation near the wall is obviously due to chain connectivity effects. Note that the block formation does not seem to be captured by the theoretical predictions.

To obtain a clearer view on the adsorption behavior of the polymerizing lattice fluid, we have depicted an overview for box filling fraction $\eta$ = 0.5 in Figures 8 and 9, where respectively the normalized packing fractions in the first and second layer are plotted versus the strength of the interaction between the associating particles. From Figure 8 it is seen that the theory and the simulations roughly have the same dependence of $g(1)$ on $u_{\text{attr}}$. Note that although there is an accumulation ($g(1) > 1$) of associating particles at the wall for $u_{\text{w}} = -0.25k_{\text{B}}T$ (●), there is a decrease of the adsorption for increasing $|u_{\text{attr}}|$. This was also observed in Figure 4 for the adsorption of the dimerizing fluid at a wall with $u_{\text{w}} = -0.25k_{\text{B}}T$. The decrease of $g(1)$ with increasing $u_{\text{attr}}$ can be attributed to a higher entropic penalty that the wall imposes on a fluid of longer chains. It is seen from Figures 4 and 8 that the decrease of $g(1)$ with $u_{\text{attr}}$ is more pronounced for the doubly associating fluid, which was to be expected because association is much more important in polymerizing fluids.

From Figure 9 it is seen that the theory is also qualitatively correct for $g(2)$ if the wall is non-interacting (●), although the dependence of $g(2)$ on $u_{\text{attr}}$ predicted by the theory is too strong. For the interacting wall (■) the theory and the simulations appear to behave differently. The simulations show an increase of the adsorbed amount in the second layer, whereas the theory shows a maximum. Note that the decrease of $g(1)$ (● in Figure 8) and the increase of $g(2)$ (■ in Figure 9) for $u_{\text{w}} = -0.25k_{\text{B}}T$ lead to the block profiles observed in Figures 6 and 7. It is seen in Figures 8 and 9 that, in the simulations for $u_{\text{w}} = -0.25k_{\text{B}}T$ (●), the decrease in $g(1)$ and the increase in $g(2)$ flatten for higher $u_{\text{attr}}$. It is most likely that for a certain $u_{\text{attr}}$ they will reach respectively a maximum and a minimum value, simply because it is improbable that the packing fraction in the second layer will surpass the packing fraction in the first layer. For higher $|u_{\text{attr}}|$ we can certainly expect to monitor an increase of $g(3)$ with increasing $|u_{\text{attr}}|$, although this increase will be shifted toward higher $|u_{\text{attr}}|$ when compared to that of $g(2)$. The increase of $g(3)$ corresponds to the formation of an adsorbed layer that extends deeper into the fluid if the average length of the molecules is increased.

The theory for the adsorption of a polymerizing fluid, for which some results have been presented in this subsection, is based on a precise diagrammatical analysis of the wall–fluid and fluid–fluid correlations. Despite this fact, the results are at most qualitatively correct. Reasons must lie in the approximations that were made to obtain a solvable set of equations for the bulk correlations of the polymerizing fluid. These approximations are the assumption of independence of the interaction sites on each particle and the preaveraging of the site–site potential $u_{\text{attr}}(1,2)$ over the orientations of $s_1$ and $s_2$ in the closure and mass balance equations for the bulk correlations. Another reason could in principle be the approximate nature of the closure equations, but this is less likely because the closures have proven to function very well in the calculation of the adsorption profiles of dimerizing fluids, as was shown in the previous subsection.

6. Conclusions

Cubic lattice models of singly and doubly associating fluids have been studied to assess the adsorption behavior of dimerizing and polymerizing fluids at impenetrable interacting walls. The method that was employed is based on Wertheim’s OZ formalism and offers an elegant, relatively simple approach to study the adsorption behavior of associating lattice fluids.

The concentration profiles that were obtained have been tested with Monte Carlo simulations. The simulation of the doubly associating lattice fluid employed a biased cluster move.

The overall agreement between the theory and the simulations is quantitative for the singly associating fluid. These results therefore suggest that Wertheim’s OZ matrix formalism is also suitable for accurately study polymerizing fluids. Unfortunately, the results obtained for polymerizing fluids indicate that better approximations have to be adopted in solving the equations that result from Wertheim’s formalism: we do not find quantitative but only qualitative agreement for the adsorption profiles at a non-interacting wall. The adsorption of the polymerizing fluid at an interacting wall seems to be incorrectly described by the theory. The simulations show the formation of a block profile, whereas the theory shows a smoothly decreasing adsorption profile.

Finally, the method presented here forms an alternative to the (polymer) RISM and other approaches to study polymer adsorption. The method does, contrary to the polymer RISM approach, not use the concept of an intramolecular distribution function to capture the conformations of the molecules near the interface, and incorporates polydispersity in an elegant way.

Figure 8. Normalized packing fraction, $g(1)$, in the layer closest to the wall, versus associative interaction strength. Symbols are simulation results, and lines are calculated results: (●) $u_{\text{w}} = -0.25k_{\text{B}}T$; (○) $u_{\text{w}} = 0.0k_{\text{B}}T$.

Figure 9. Caption as in Figure 8, but for the next nearest neighbor layer to the wall.
Appendix: Solution Scheme

Here, we outline the method for obtaining the $h_l(l)$ from eqs 11–15 for known $h_l(l,m,n)$ and $c_l(l,m,n)$. Solution of eq 11 is conveniently performed in Fourier space. Therefore, we apply the 1D Fourier transform

$$\hat{f}(u) = \sum_l f(l) \cos lu$$  \hspace{1cm} (29)$$
with inverse

$$f(l) = \frac{1}{2\pi} \int_{-\pi}^{\pi} \hat{f}(u) \cos lu \, du$$  \hspace{1cm} (30)$$

If it is assumed that the concentration profile is the same on both sides of the wall, i.e., $h_l(+l) = h_l(-l)$, we can write eq 11 as

$$\hat{h}_l(u) = \hat{c}_l(u) + (\eta \hat{h}_0(u,0,0) + \eta_0 \hat{h}_1(u,0,0)) \hat{\xi}_0(u) + \eta_0 \hat{h}_0(u,0,0) \hat{\xi}_1(u)$$  \hspace{1cm} (31)$$

where the $\hat{h}_l(u,0,0)$ are given by 3D Fourier transform

$$\hat{f}(u,v,w) = \sum_{l,m,n} f(l,m,n) \cos lu \cos mv \cos nw$$  \hspace{1cm} (32)$$

and

$$f(l,m,n) = \left( \frac{1}{2\pi} \right)^3 \int_{-\pi}^{\pi} \int_{-\pi}^{\pi} \int_{-\pi}^{\pi} \hat{f}(u,v,w) \cos lu \cos mv \times \cos nw \, du \, dv \, dw$$ \hspace{1cm} (33)$$

for $v = 0$ and $w = 0$.

The $\hat{h}_l(u,0,0)$ in eq 31 can be obtained separately from the solution of the bulk equations.\textsuperscript{23} Once the $\hat{h}_l(u,0,0)$ are known, a numerically simple problem in four unknowns ($c_l(0), c_l(1), c_l(0)$, and $c_l(1)$) results. The unknowns are found as follows.

From eq 15 and the closures, eqs 12 and 13, we obtain the nonoverlap conditions

$$h_l(0) = -\delta_{l0}$$  \hspace{1cm} (34)$$
and the contact relations

$$c_l(1) = (h_l(1) + \delta_{l0})(1 - e^{\alpha w})$$  \hspace{1cm} (35)$$

Note that the partial direct correlation functions $c_l(l)$ are only nonzero for $l \leq 1$. This is a direct consequence of the use of the Percus–Yevick-like closure, eq 12, and limits the number of unknowns to four.

The unknowns are now directly found from equations that result from combining eqs 30, 31, 34, and 35

$$-\delta_{l0} = \frac{1}{2\pi} \int_{-\pi}^{\pi} \hat{h}_l(u) \, du$$

$$\frac{c_l(1)}{1 - e^{\alpha w}} - \delta_{l0} = \frac{1}{2\pi} \int_{-\pi}^{\pi} \hat{h}_l(u) \cos u \, du$$  \hspace{1cm} (36)$$

with $\hat{c}_l(u) = c_l(0) + 2c_l(1) \cos u$, according to eq 29. The $c_l(0)$ and $c_l(1)$ are obtained from eq 36 with a Newton–Raphson procedure combined with a 1D quadrature routine. Once the unknowns are found, we obtain the $h_l(l)$ from eqs 30 and 31 for $f = h_l$.

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