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Cu Cu -1.9646 0.5888 'International Tables Vol C Tables 4.2.6.8 and 6.1.1.4'

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_symmetry_equiv_pos_as_xyz

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 'x-y, x, z+1/2'
 'y, x, -z'
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Refinement of F^2 against ALL reflections. The weighted R-factor wR and goodness of fit S are based on F^2 , conventional R-factors R are based on F , with F set to zero for negative F^2 . The threshold expression of $F^2 > 2\sigma(F^2)$ is used only for calculating R-factors(gt) etc. and is not relevant to the choice of reflections for refinement. R-factors based on F^2 are statistically about twice as large as those based on F , and R-

factors based on ALL data will be even larger.

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SQUEEZE RESULTS (APPEND TO CIF)

Note: Data are Listed for all Voids in the P1 Unit Cell

i.e. Centre of Gravity, Solvent Accessible Volume,

Recovered number of Electrons in the Void and

Details about the Squeezed Material

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1 -0.043 -0.028 -0.002 6581 1531 ''

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_atom_sites_solution_secondary difmap

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O2 O 0.62863(17) 0.10934(15) -0.00239(8) 0.1007(9) Uani 1 1 d . . .
O3 O 0.43644(18) -0.1271(4) 0.08185(15) 0.174(2) Uani 1 2 d S . .
C1 C 0.6395(3) 0.0906(2) 0.03153(11) 0.0923(12) Uani 1 1 d . . .
C2 C 0.77847(19) 0.22153(19) 0.03237(14) 0.0906(16) Uani 1 2 d S . .
H2A H 0.7684 0.2316 0.0070 0.109 Uiso 1 2 calc SR . .
C3 C 0.7209(3) 0.1491(2) 0.05100(10) 0.0937(12) Uani 1 1 d . . .
C4 C 0.7364(3) 0.1343(3) 0.08877(10) 0.1064(14) Uani 1 1 d . . .
H4A H 0.6980 0.0855 0.1014 0.128 Uiso 1 1 calc R . .
C5 C 0.8085(2) 0.1915(2) 0.10784(14) 0.110(2) Uani 1 2 d S A .
C6 C 0.8207(3) 0.1793(3) 0.15062(16) 0.117(2) Uani 1 2 d S . .
C7 C 0.7963(9) 0.0960(7) 0.1633(2) 0.165(5) Uani 0.50 1 d P A 1
H7A H 0.7760 0.0525 0.1454 0.198 Uiso 0.50 1 calc PR A 1
C8 C 0.8031(8) 0.0799(7) 0.2027(2) 0.162(5) Uani 0.50 1 d P A 1
H8A H 0.7868 0.0270 0.2124 0.194 Uiso 0.50 1 calc PR A 1
C7' C 0.8381(6) 0.2441(6) 0.1762(2) 0.122(3) Uani 0.50 1 d P A 2
C8' C 0.8394(6) 0.2220(6) 0.2171(2) 0.121(4) Uani 0.50 1 d P A 2
C9 C 0.8405(4) 0.1595(4) 0.2282(2) 0.160(3) Uani 1 2 d S . .
C10 C 0.8508(11) 0.2848(10) 0.2500 0.131(6) Uani 0.50 2 d SP . .
C11 C 0.9398(13) 0.3597(10) 0.2500 0.168(7) Uani 0.50 2 d SP A .
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O2 0.113(2) 0.0746(16) 0.0857(16) 0.0003(13) 0.0014(15) 0.0255(15)
O3 0.197(4) 0.172(5) 0.144(4) 0.096(4) 0.0481(19) 0.086(2)
C1 0.107(3) 0.074(2) 0.073(2) -0.005(2) 0.004(2) 0.028(2)
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C3 0.101(3) 0.086(3) 0.063(2) -0.0078(19) 0.0005(19) 0.023(2)
C4 0.109(3) 0.093(3) 0.072(2) -0.002(2) 0.001(2) 0.016(2)
C5 0.113(3) 0.113(3) 0.057(3) -0.0004(17) 0.0004(17) 0.020(4)
C6 0.118(3) 0.118(3) 0.067(3) 0.003(2) -0.003(2) 0.024(4)
C7 0.234(13) 0.113(8) 0.062(5) 0.004(5) -0.003(6) 0.023(8)
C8 0.239(13) 0.128(8) 0.061(4) -0.003(5) 0.007(6) 0.049(9)
C7' 0.140(8) 0.128(7) 0.063(4) -0.018(5) -0.005(5) 0.040(6)
C8' 0.149(9) 0.079(6) 0.071(5) -0.005(4) 0.019(5) 0.008(5)
C9 0.201(7) 0.201(7) 0.070(4) -0.005(3) 0.005(3) 0.094(9)
C10 0.161(14) 0.123(11) 0.058(6) 0.000 0.000 0.031(11)
C11 0.221(19) 0.101(11) 0.107(9) 0.000 0.000 0.025(12)
C12 0.27(3) 0.23(3) 0.123(11) 0.000 0.000 0.18(3)

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All esds (except the esd in the dihedral angle between two l.s. planes) are estimated using the full covariance matrix. The cell esds are taken into account individually in the estimation of esds in distances, angles and torsion angles; correlations between esds in cell parameters are only used when they are defined by crystal symmetry. An approximate (isotropic) treatment of cell esds is used for estimating esds involving l.s. planes.

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Cu1 O2 1.946(3) 8 ?

Cu1 O1 1.950(3) 20_655 ?

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Cu1 O3 2.154(4) . ?

Cu1 Cu1 2.6462(13) 13_655 ?

O1 C1 1.267(4) . ?

O2 C1 1.263(4) . ?

O2 Cu1 1.946(3) 13_655 ?

C1 C3 1.501(5) . ?

C2 C3 1.383(4) . ?

C2 C3 1.383(4) 19_665 ?

C3 C4 1.389(5) . ?

C4 C5 1.384(5) . ?

C5 C4 1.384(5) 19_665 ?

C5 C6 1.525(7) . ?

C6 C7' 1.389(10) . ?

C6 C7' 1.389(10) 19_665 ?

C6 C7 1.438(12) 19_665 ?

C6 C7 1.439(12) . ?

C7 C8 1.408(12) . ?

C7 C7 1.99(2) 19_665 ?

C8 C9 1.548(12) . ?

C7' C8' 1.472(11) . ?

C7' C7' 1.520(19) 19_665 ?

C7' C8' 1.973(12) 19_665 ?

C8' C8' 1.136(17) 19_665 ?

C8' C9 1.227(12) . ?

C8' C10 1.559(14) . ?

C8' C7' 1.973(12) 19_665 ?

C9 C8' 1.227(12) 19_665 ?

C9 C9 1.500(14) 16_556 ?

C9 C8 1.548(12) 19_665 ?

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C7' C8' C10 120.3(9) . . ?
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C8' C9 C8' 55.1(11) . 19_665 ?
C8' C9 C9 108.2(6) . 16_556 ?
C8' C9 C9 108.2(6) 19_665 16_556 ?
C8' C9 C8 120.5(9) . . ?
C8' C9 C8 82.0(8) 19_665 . ?
C9 C9 C8 124.6(4) 16_556 . ?
C8' C9 C8 82.0(8) . 19_665 ?
C8' C9 C8 120.5(9) 19_665 19_665 ?
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