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## ON COSMIC-RAY PRODUCTION EFFICIENCY AT SUPERNOVA REMNANT SHOCKS PROPAGATING INTO REALISTIC DIFFUSE INTERSTELLAR MEDIUM

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### ABSTRACT

Using three-dimensional magnetohydrodynamics simulations, we show that the efficiency of cosmic-ray (CR) production in supernova remnants is over-predicted if it could be estimated based on proper motion measurements of H $\alpha$  filaments in combination with shock-jump conditions. Density fluctuations of the upstream medium cause shock waves to be rippled and oblique almost everywhere. The kinetic energy of the shock wave is transferred into downstream turbulence as well as thermal energy related to the shock velocity component normal to the shock surface. Our synthetic observation shows that the CR acceleration efficiency, as estimated from a lower downstream plasma temperature, is overestimated by 10%–40% because a rippled shock does not immediately dissipate all of the upstream kinetic energy.

*Key words:* acceleration of particles – ISM: supernova remnants – proper motions – shock waves – turbulence

### 1. INTRODUCTION

The energy density of Galactic cosmic rays (CRs) around the Earth is explained if 1%–10% of supernova explosion energy is used for CR acceleration. The CR production efficiency in supernova remnants (SNRs) has been widely discussed and seems to be ubiquitously so high that the back reaction of CRs onto the background shock structure is significant. One way to estimate the CR production efficiency is through a combination of measurements of the proper motion of the shock front and the temperature of the shocked gas (e.g., Hughes et al. 2000; Tatischeff & Hernanz 2007; Helder et al. 2009; Morlino et al. 2013, 2014). The expansion speed of the SNR has been measured in various wavelengths, from which the downstream temperature  $T_{\text{proper}}$  is predicted using the Rankine–Hugoniot shock-jump condition. If the actual downstream temperature  $T_{\text{down}}$  can be independently measured, then the CR production efficiency  $\eta$  is given by

$$\eta = \frac{T_{\text{proper}} - T_{\text{down}}}{T_{\text{proper}}}, \quad (1)$$

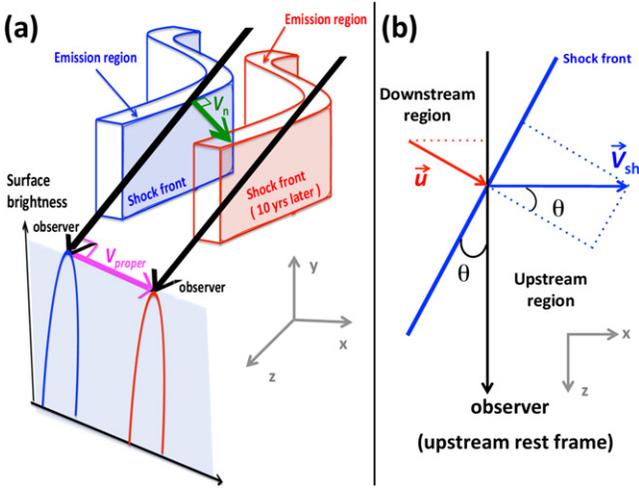
where we assume that all of the missing thermal energy goes into CR production. Note that  $\eta$  can be related to  $\beta$  which was given by Equation (22) of Vink et al. (2010) as  $\eta = 1 - \beta$ . Observations of the northeast region of the young SNR RCW 86 gives us an example. The proper motion velocity of the synchrotron X-ray filaments is measured as  $\sim 6000 \pm 2800 \text{ km s}^{-1}$  (Helder et al. 2009), while those of the H $\alpha$  filaments range from 300 to 3000  $\text{km s}^{-1}$  with a mean of 1200  $\text{km s}^{-1}$  (Helder et al. 2013). Let the expansion speed of the SNR be 3000  $\text{km s}^{-1}$  so that the X-ray and H $\alpha$  observations are consistent with each other. If the proper motion velocity is equivalent to the shock velocity, then the downstream proton temperature is predicted by the Rankine–Hugoniot relation as  $T_{\text{proper}} = 17.6 \text{ keV}$ . This value is different from the direct measurement,  $T_{\text{down}} = 2.3 \pm 0.3 \text{ keV}$ , given by the line width of the broad

component of the H $\alpha$  emission (Helder et al. 2009). Then, we obtain  $\eta \approx 87\%$  which suggests extremely efficient CR acceleration. Even if the shock velocity is as low as 1200  $\text{km s}^{-1}$ , the efficiency is 18%.

In previous discussions, it was assumed that the shock was plane parallel—that is, that the shock normal is parallel to the flow—and that the measured proper motion velocity was identical to the shock velocity. These assumptions would be suitable for a spherically symmetric shock wave propagating into a homogeneous medium. However, they may not be true for actual SNRs. The observed velocity of the proper motion of H $\alpha$  filaments is dispersed (e.g., Helder et al. 2013), which implies shock propagation through an inhomogeneous medium. At present, it is widely accepted that the interstellar medium is highly inhomogeneous (e.g., de Avillez & Breitschwerdt 2007), in particular, near young SNRs (e.g., Fukui et al. 2003; Moriguchi et al. 2005). So far, we have investigated the effects of upstream inhomogeneity and shown that various observational results can be explained (Inoue et al. 2009, 2010, 2012, 2013). Some predictions of magnetohydrodynamics (MHD) simulations regarding magnetic field amplification due to a turbulent dynamo downstream (Giaccalone & Jokipii 2007; Inoue et al. 2009, 2012; Sano et al. 2012) have been observationally confirmed (Bamba et al. 2003, 2005a, 2005b; Vink & Laming 2003; Yamazaki et al. 2004; Uchiyama et al. 2007; Sano et al. 2013, 2014). In this paper, we will show that the above approximations may lead to overestimates of the CR production efficiency in SNRs. In order to study the influence of upstream inhomogeneities, we perform a three-dimensional (3D) MHD simulation of a shock wave propagating into an inhomogeneous medium, and we simulate H $\alpha$  filaments whose proper motion is synthetically measured.

### 2. SHOCK PROPAGATION THROUGH AN INHOMOGENEOUS ISM

Multi-dimensional MHD simulations of shock propagation through an inhomogeneous diffuse ISM with a Kolmogorov-



**Figure 1.** (a) Relation between proper motion velocity and the velocity component normal to the shock surface for a rippled shock. The curved blue sheet represents a part of the rippled shock front and the emission region of  $\text{H}\alpha$ . The curved red sheet also represents those after a short-time propagation. Thick black arrows show LOSs. A limb brightening effect causes a peaked profile in surface brightness as shown in the inner panel. The magenta and green vectors represent the observed proper motion velocity  $V_{\text{proper}}$  and the velocity component normal to the shock surface  $V_n$ , respectively. One can see that  $V_{\text{proper}}$  is generally larger than  $V_n$ . (b) Enlarged view of the local oblique shock. The blue line represents the shock front that propagates along the  $x$  axis, and the LOS direction (black arrow) is taken along the  $z$  axis. In the upstream rest frame, the downstream fluid velocity  $\mathbf{u}$  is definitively parallel to the shock normal. The  $z$  component of  $\mathbf{u}$  causes the Doppler shift in the broad  $\text{H}\alpha$  line emission from this region.

like density power spectrum have shown that the shock front is rippled due to the fluctuating inertia of the preshock ISM (see Giacalone & Jokipii 2007 for the 2D case and Inoue et al. 2013 for the 3D case). Their results strongly suggest that an SNR forward shock is locally oblique. For oblique shocks, the downstream temperature is given by the velocity component normal to the shock surface  $V_n$  (not the shock velocity itself):

$$k_B T_{\text{down}} = \frac{3}{16} m_p V_n^2, \quad (2)$$

where  $k_B$  and  $m_p$  are the Boltzmann constant and proton mass, respectively. The velocity measured by the proper motion is identical to the shock velocity component transverse to line of sight (LOS). Thus, when the shock front is rippled, the proper motion velocity,  $V_{\text{proper}}$ , can be larger than  $V_n$ . In Figure 1(a), we illustrate this situation. The blue curved sheet represents part of the rippled shock front emitting  $\text{H}\alpha$  photons. As seen in the bottom of the figure, the limb brightening effect causes a peaked profile in the surface brightness on the celestial sphere (Hester 1987). As the shock propagates, the peak of the brightness moves outward (red sheet), which is observed as proper motion in the celestial sphere (magenta vector). Since  $V_{\text{proper}} \geq V_n$ , the downstream temperature calculated based on the proper motion measurement can be overestimated, i.e.,  $T_{\text{proper}} = 3 m_p V_{\text{proper}}^2 / (16 k_B) \geq T_{\text{down}}$ , so that  $\eta$  is apparently non-zero in spite of no CR acceleration. In the following, using the result of a 3D MHD simulation of a shock propagating through an inhomogeneous medium performed by Inoue et al. (2013), we demonstrate that the above expectation is generally realized.

### 3. SET UP OF MHD SIMULATION

In this paper, we use the data from the simulation performed by Inoue et al. (2013). Here, we briefly summarize the set up of the simulation by Inoue et al. (2013). They studied shock propagation into an inhomogeneous medium parameterized by the amplitude of the density fluctuation  $\Delta\rho/\langle\rho\rangle_0$  assuming ideal MHD with adiabatic index  $\gamma = 5/3$  and a mean molecular weight of 1.27, where  $\langle\rho\rangle_0$  is the initial mean density and  $\Delta\rho \equiv (\langle\rho^2\rangle - \langle\rho\rangle_0^2)^{1/2}$  is the dispersion. The fluctuations are given as a superposition of the sinusoidal functions with various wave numbers ( $2\pi/L_{\text{box}} \leq |k| \leq 256\pi/L_{\text{box}}$ ). The simulation is performed in a cubic numerical domain with volume  $L_{\text{box}}^3 = (2 \text{ pc})^3$  which is resolved by  $(1024)^3$  unit cells. The power spectrum of the density fluctuations is given by the isotropic power law,  $R_D(k) \equiv \rho_k^2 k^2 \propto k^{-5/3}$ , for the above range of  $k$ , where  $\rho_k$  is the Fourier component of the density. The above Kolmogorov spectrum is consistent with the observed big-power-law-in-the-sky (Armstrong et al. 1995).

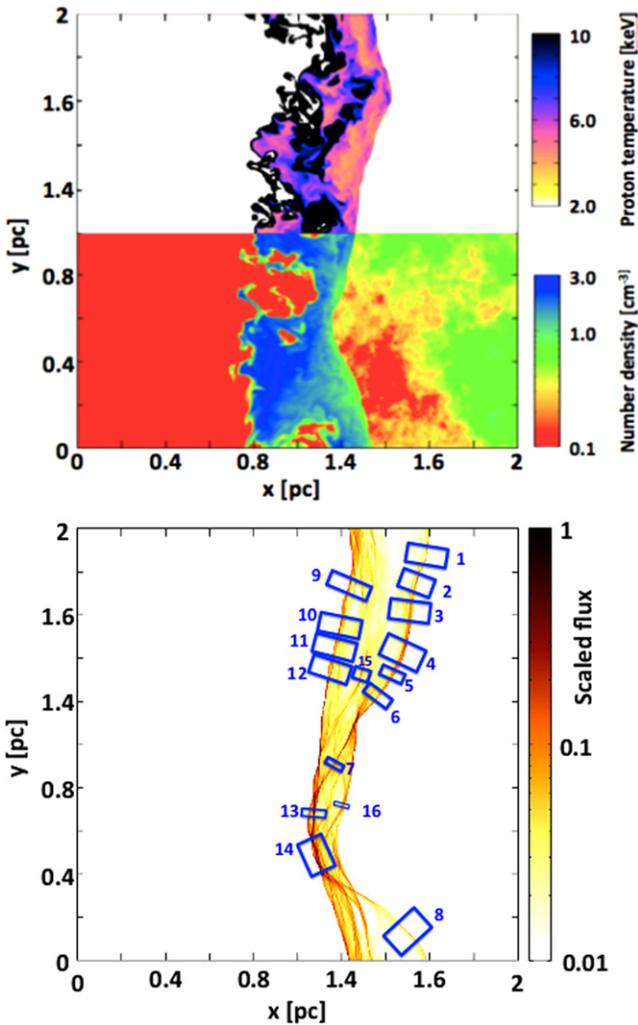
The initial mean number density, thermal pressure, and magnetic field strength are set to be  $\langle n \rangle_0 = 0.5 \text{ cm}^{-3}$ ,  $P/k_B = 4 \times 10^3 \text{ K cm}^{-3}$ , and  $B_0 = 3.0 \mu\text{G}$ , respectively. These are the typical values in the diffuse ISM (Myers 1978; Beck 2000). Thus, the initial mean sound speed and Alfvén velocity are  $\langle c_s \rangle = 9.3 \text{ km s}^{-1}$  and  $\langle c_A \rangle = 8.2 \text{ km s}^{-1}$ , respectively. To induce a blast wave shock, we set the hot plasma to  $p_h/k_B = 2 \times 10^8 \text{ K cm}^{-3}$ ,  $n_h = 0.05 \text{ cm}^{-3}$ , and  $B_h = 3.0 \mu\text{G}$  at the  $x = 0$  boundary plane. The resulting mean propagation speed of the shock is  $1800 \text{ km s}^{-1}$ , which is suitable for studying young SNRs, although the local shock velocity has a large dispersion due to shock rippling.

In this paper, we use data from the simulation for  $\Delta\rho/\langle\rho\rangle_0 = 0.3$ , which can be regarded as a typical ISM model. The reason for this is as follows. If we suppose that the turbulence in the ISM is driven by supernovae, then the driving scale of the turbulence and the degree of density fluctuation at the driving scale would be given as  $L_{\text{inj}} \sim 100 \text{ pc}$  and  $\Delta\rho/L_{\text{inj}}/\langle\rho\rangle_0 \sim 1$ , respectively (e.g., de Avillez & Breitschwerdt 2007). In that case, the degree of small-scale density fluctuations due to the cascade of the turbulence at a scale of  $L_{\text{box}} = 2 \text{ pc}$  is estimated as  $\Delta\rho/L_{\text{inj}}/\langle\rho\rangle_0 \simeq (L_{\text{box}}/L_{\text{inj}})^{1/3} \sim 0.3$ .

### 4. RESULTS OF MHD SIMULATION AND SYNTHETIC OBSERVATIONS

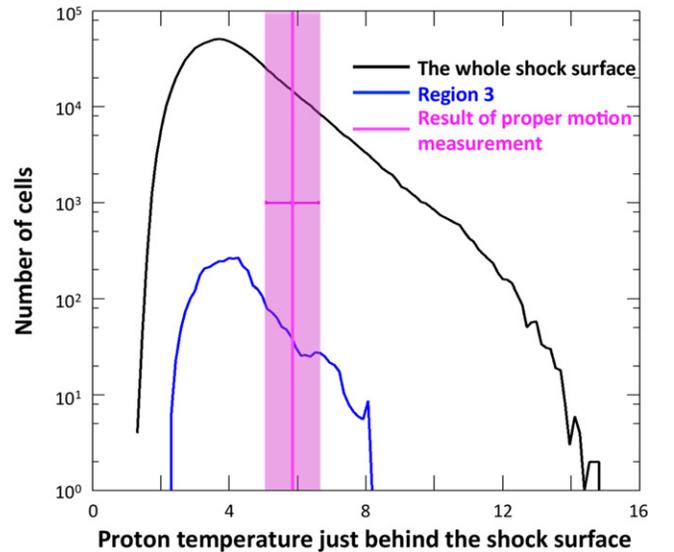
In this section, we show our simulation results. The top panel of Figure 2 represents the two-dimensional slice of the proton temperature (*upper half*) and the number density (*lower half*) in the  $t_{\text{obs}} = 700 \text{ yr}$  and  $z = 0 \text{ pc}$  plane. The proton temperature is estimated from  $T_p = P/(\rho k_B)$ , where  $P$  and  $\rho$  are the pressure and density. From Figure 2, we observe that shock waves propagate into the realistic ISM with various angles and velocities. As a result, the temperature distribution is inhomogeneous (see the black curve of Figure 3). In this inhomogeneous system, it may be that the relation between the proper motion velocity of  $\text{H}\alpha$  and the downstream temperature does not satisfy the Rankine–Hugoniot relations.

In order to estimate the deviation from the Rankine–Hugoniot relations, we calculate the proper motion of the  $\text{H}\alpha$  emission over 10 yr (from  $t_{\text{obs}} = 700$  to 710 yr). The  $\text{H}\alpha$



**Figure 2.** (Top panel) two-dimensional slice of the proton temperature (*upper half*) and number density (*lower half*) in the  $t_{\text{obs}} = 700$  yr and  $z = 0$  pc plane. (Bottom panel) simulated H $\alpha$  image. We set the LOS along the  $z$  axis. Color represents the scaled flux of H $\alpha$ . We selected 16 local regions (*blue box*) in which the proper motion of the H $\alpha$  filament is measured to predict the downstream proton temperature.

emission observed from SNRs sometimes has narrow and broad components. The former is a characteristic of the cold interstellar medium which arises from direct excitation of the neutral hydrogen atoms crossing the shock surface. The latter is a characteristic of the thermal broadening of the shocked protons which arises from hot hydrogen atoms generated by a charge exchange reaction between cold neutrals and shocked protons. In this paper, we calculate only the narrow component of the H $\alpha$  emission from our MHD simulation because the broad component of H $\alpha$  is not necessarily observed from SNRs. We consider hydrogen atoms, electrons, and protons as particles. The results of our MHD simulation are valid as long as the ionization fraction of the upstream gas is sufficiently high because our MHD simulation does not take into account the ionization of neutral hydrogen atoms. Recent studies have shown that the ionization of neutral hydrogen atoms changes the collisionless shock structures (Ohira et al. 2009; Ohira & Takahara 2010; Ohira 2012, 2013, 2014; Blasi et al. 2012). Therefore, we consider a highly ionized upstream gas in this paper because the effects of ionization can be neglected.



**Figure 3.** Distributions of the proton temperature of the fluid cell just behind the shock surface. The black curve is for the whole shock surface, while the blue is for the surface of the LOS crossing the H $\alpha$  filament of Region 3. The vertical magenta line represents the downstream proton temperature,  $T_{\text{proper}}$ , which is inferred from the best-fit proper motion velocity with the magenta belt showing the associated error.

According to Heng & McCray (2007), the rate (in units of  $\text{s}^{-1}$ ) that hydrogen atoms (denoted H) will have a reaction  $X$  ( $X = E, I,$  and  $CE$  for excitation, ionization, and charge exchange) with particles of type  $s$  ( $s = e$  and  $p$  for electrons and protons, respectively) is given by

$$R_{X,s} = n_s \int d^3v_H \int d^3v_s f_H(v_H) f(v_s) \Delta v_s \sigma_{X,s}(\Delta v_s), \quad (3)$$

where  $n_s$ ,  $v_s$ , and  $f_s$  are the number density, the velocity, and the distribution function for *particle*  $s$ , respectively. The velocity and distribution function of hydrogen atoms are described as  $v_H$  and  $f_H$ , respectively. The relative velocity between neutral hydrogen atoms and *particle*  $s$  is denoted by  $\Delta v_s = |v_H - v_s|$ . We assume that distribution functions for each particle are represented by

$$f_H = \delta(v_H), \quad (4)$$

$$f_s = \left( \frac{m_s}{2\pi k_B T_s(\mathbf{r})} \right)^{3/2} \exp \left( -\frac{m_s v_s^2(\mathbf{r})}{2k_B T_s(\mathbf{r})} \right), \quad (5)$$

where  $v_s(\mathbf{r}) = |v_s - \mathbf{u}(\mathbf{r})|$  and  $\mathbf{u}(\mathbf{r})$  is the downstream fluid velocity. We regard the distribution function of hydrogen atoms as a Dirac delta function because we only consider the narrow component. In addition, we assume that the distribution functions of protons and electrons are Maxwellian with  $T_p = P/(\rho k_B)$  and  $T_e = 0.01 T_p$ , respectively (Ohira & Takahara 2007, 2008; Rakowski et al. 2008). In order to calculate Equation (3), we use our MHD simulation data for  $u(\mathbf{r})$ ,  $T_p(\mathbf{r})$ , and  $n_s(\mathbf{r})$ , as well as the data of Janev & Smith (1993) for cross sections. Calculating the excitation rate,  $R_E = R_{E,p} + R_{E,e}$ , for each cell of our MHD simulation and integrating  $n_H(\mathbf{r}) R_E(\mathbf{r})$  along the LOS ( $z$  axis), we obtain the surface emissivity of the

**Table 1**  
Calculation Results for Selected 16 Regions

Region	$V_{\text{proper}} (10^8 \text{ cm s}^{-1})$	$T_{\text{proper}} (\text{keV})$	Case 1		Case 2	
			$T_{\text{down}} (\text{keV})$	$\eta$	$T_{\text{down}} (\text{keV})$	$\eta$
1	1.8 ± 0.1	6.0 ± 0.5	5.7	0.06 ± 0.07	5.5	0.08 ± 0.07
2	1.8 ± 0.0	6.6 ± 0.3	6.0	0.09 ± 0.04	5.7	0.14 ± 0.04
3	1.7 ± 0.1	5.8 ± 0.8	4.2	0.27 ± 0.09	3.9	0.33 ± 0.08
4	1.4 ± 0.1	3.7 ± 0.4	3.0	0.19 ± 0.08	2.9	0.22 ± 0.07
5	1.4 ± 0.1	3.7 ± 0.4	2.6	0.28 ± 0.08	2.6	0.29 ± 0.08
6	1.4 ± 0.0	4.0 ± 0.2	2.9	0.28 ± 0.04	2.8	0.30 ± 0.03
7	1.4 ± 0.1	3.9 ± 0.6	3.3	0.20 ± 0.10	3.1	0.20 ± 0.11
8	1.7 ± 0.1	5.4 ± 0.6	4.1	0.24 ± 0.08	3.9	0.28 ± 0.08
9	2.0 ± 0.1	7.5 ± 0.9	5.1	0.32 ± 0.07	4.9	0.34 ± 0.07
10	2.1 ± 0.0	8.2 ± 0.2	5.5	0.33 ± 0.02	5.2	0.36 ± 0.02
11	2.0 ± 0.0	8.2 ± 0.3	5.2	0.37 ± 0.02	5.0	0.39 ± 0.02
12	1.9 ± 0.1	7.2 ± 0.6	4.3	0.40 ± 0.05	4.3	0.41 ± 0.05
13	1.6 ± 0.1	5.2 ± 0.5	3.5	0.33 ± 0.06	3.4	0.35 ± 0.06
14	1.6 ± 0.1	5.0 ± 0.6	4.3	0.10 ± 0.10	3.9	0.22 ± 0.09
15	1.4 ± 0.1	4.0 ± 0.4	2.9	0.27 ± 0.07	2.9	0.29 ± 0.07
16	2.0 ± 0.0	8.2 ± 0.1	7.2	0.11 ± 0.01	7.7	0.06 ± 0.01
Mean/std. dev.	1.7/0.24	5.8/1.6	4.4/1.3	0.24/0.10	4.2/1.3	0.27/0.10

H $\alpha$  emission,

$$S(x, y) = \int n_{\text{H}}(\mathbf{r}) R_E(\mathbf{r}) dz, \quad (6)$$

where we consider only direct excitation from the ground state to the  $n = 3$  level. Neutral hydrogen atoms are ionized in the downstream region. The density of neutral hydrogen atoms in the downstream region is given by

$$n_{\text{H}}(\mathbf{r}) = n_{\text{H},0}(\mathbf{r}) \exp[-R_I(\mathbf{r})(t_{\text{obs}} - t_{\text{sh}}(\mathbf{r}))], \quad (7)$$

where  $R_I(\mathbf{r}) = R_{I,p}(\mathbf{r}) + R_{\text{CE},p}(\mathbf{r}) + R_{I,e}(\mathbf{r})$  and  $t_{\text{sh}}(\mathbf{r})$  is the time when the shock wave passes through point  $\mathbf{r}$ . For the initial hydrogen density,  $n_{\text{H}}$ , we assume that the initial ionization fraction of the ISM is uniform. The bottom panel of Figure 2 is the H $\alpha$  image obtained from Equations (3)–(7).

As shown in the bottom panel of Figure 2, we select 16 regions which contain clear filamentary structure of H $\alpha$  to measure proper motion. We extract a surface brightness profile from these regions and analyze their proper motions in the same way as Helder et al. (2013). To measure the proper motion, we shift the normalized profiles over one another in steps of one bin, calculating the  $\chi^2$  values for each shift. The length of one bin is taken as  $1.9 \times 10^{15}$  cm, which is comparable to the angular resolution of the optical instrument for the typical distance to the source of a few kiloparsecs. The best-fitting shift is determined by fitting a parabola to the three  $\chi^2$  values surrounding the minimal  $\chi^2$ . We estimate the  $1\sigma$  uncertainties on the best-fit proper motion, which correspond to  $\Delta\chi^2 = 1$ . Then, the best-fit proper motion velocity  $V_{\text{proper}}$  is related to  $T_{\text{proper}}$  as  $T_{\text{proper}} = 3m_p V_{\text{proper}}^2 / 16k_B$ , which is the same as in previous actual observational studies.

In order to evaluate  $\eta$  from Equation (1), we calculate the downstream proton temperature  $T_{\text{down}}$  in two ways. First, we take  $T_{\text{down}}$  as the mean of the downstream temperatures of fluid cells just behind the shock surface of the LOS crossing the H $\alpha$  filament (Case 1). As a typical example, in Figure 3, we show the distributions of the proton temperature  $T_{\text{down}}$  of the fluid cell

just behind the shock surface; the black curve represents the whole shock surface, while the blue represents the surface on the LOS crossing the H $\alpha$  filament of Region 3. Note that the proper motion velocity of Region 3 corresponds to the mean of our 16 regions (see Table 1). The vertical magenta line represents  $T_{\text{proper}}$  for Region 3 with the magenta belt showing the associated error. The value of  $T_{\text{proper}}$  is higher than the mean of  $T_{\text{down}}$ . We calculate, from Equation (1), the apparent CR production efficiency as  $\eta \sim 0.3 \pm 0.1$ .

Next, we consider a situation similar to actual observations where the downstream temperature  $T_{\text{down}}$  is estimated from the line width of the broad H $\alpha$  component (Case 2). It is hard to calculate exactly the broad emission component in our model. Instead, we perform a simple, approximate calculation. We obtain  $T_{\text{down}}$  from the FWHM of the sum of the shifted Maxwellian weighted by the brightness of the broad H $\alpha$  component,  $n_{\text{H},0}(\mathbf{r})\xi_{\text{CE}}(\mathbf{r})$ , of the fluid cell at  $\mathbf{r}$  just behind the shock surface on the LOS crossing the H $\alpha$  filament, where  $\xi_{\text{CE}}(\mathbf{r}) = R_{\text{CE},p}(\mathbf{r})[R_{I,p}(\mathbf{r}) + R_{I,e}(\mathbf{r})]^{-1}$ . Then, we find that  $\eta$  becomes slightly larger than for Case 1 (Table 1). This is because the hot hydrogen atom emitting the broad H $\alpha$  component is generated by a charge exchange reaction, whose cross-section decreases rapidly if the relative velocity is higher than  $\approx 2000 \text{ km s}^{-1}$ . Thus, the observed downstream temperature may be biased against the particular temperature. This effect has already been investigated for a one-dimensional shock wave through detailed analysis of H $\alpha$  emission (van Adelsberg et al. 2008). Since a rippled shock front generates dispersion in the downstream fluid velocity, one might consider the line width to be spread by downstream bulk motion. If this Doppler effect were significant, then the measured  $T_{\text{down}}$  would tend to be higher than the actual downstream proton temperature, resulting in lower  $\eta$ . However, this is not the case for our present synthetic observation. It is known for oblique shocks that in the upstream rest frame, the downstream fluid velocity  $\mathbf{u}$  is parallel to the shock normal (Figure 1(b)). Hence, if the rippled shock front is viewed nearly edge-on as in

the present case, then the Doppler broadening is not so significant.

Table 1 shows the measured proper motion velocity and apparent CR production efficiency  $\eta$  for the 16 regions. As expected in Section 2,  $T_{\text{proper}}$  is higher than  $T_{\text{down}}$  and the efficiency  $\eta$  is positive, even though our simulations do not involve the effects of comic-ray acceleration.

## 5. DISCUSSION

We have shown that the CR production efficiency  $\eta$  seems to be overestimated in the shock wave of SNRs propagating into a realistic ISM if the post-shock temperature  $T_{\text{proper}}$  is estimated from the proper motion of the  $\text{H}\alpha$  filaments in combination with the Rankine–Hugoniot relation for a plane-parallel shock. It may not be a suitable assumption for actual SNR shocks that the shock wave is plane parallel and that the measured proper motion velocity is equivalent to the shock velocity. Density fluctuations of a realistic ISM make the rippled, locally oblique shock front almost everywhere. For the oblique shocks, the post-shock temperature is given not by the shock velocity itself but by the velocity component normal to the shock surface  $V_n$  as shown by Equation (2). Because proper motion measurements give us the velocity component transverse to the LOS (see Figure 1), the predicted post-shock temperature  $T_{\text{proper}}$  given by the Rankine–Hugoniot relation with the assumption of a plane parallel shock is larger than actual downstream temperature  $T_{\text{down}}$ . Therefore, we claim that the CR production efficiency  $\eta$  has some uncertainty and can be positive (up to 0.4 in our case) despite no CR acceleration.

As shown in the Appendix, a simple analytical argument gives the upper and lower bounds of  $\eta$  as

$$\left( \frac{\Delta\rho}{\langle\rho\rangle_0} \right)^2 \lesssim \eta \lesssim 2 \frac{\Delta\rho}{\langle\rho\rangle_0}, \quad (8)$$

where  $\Delta\rho/\langle\rho\rangle_0$  is the upstream density fluctuation at scale  $L_{\text{box}} = 2$  pc. Since we have set  $\Delta\rho/\langle\rho\rangle_0 = 0.3$  in our present simulation study, this analytical formula is roughly consistent with our numerical result. RCW 86 is likely an SNR expanding in the windblown bubble (Vink et al. 1997, 2006), and a part of the shock collided with dense clumps and/or a cavity wall very recently (Yamaguchi et al. 2008) so that we expect a larger value of  $\Delta\rho/\langle\rho\rangle_0$  than that of the ISM. If the CR acceleration is inefficient so that the nonlinear effect can be neglected, then we expect  $\Delta\rho/\langle\rho\rangle_0 \approx 0.4$  in order to explain the observational result  $\eta = 0.2\text{--}0.9$  (see Section 1). On the other hand, shock deformation in  $\sim 10$  pc scale may be smaller for SNRs such as SN 1006, Tycho’s remnant, and SNR 0509–67.5, which are embedded in the ISM with smaller  $\Delta\rho/\langle\rho\rangle_0$  than RCW 86. The global  $\text{H}\alpha$  image of SN 1006, whose radius is about 10 pc, looks like a circular ring except for the northwest region, while smaller-scale ( $\lesssim$  a few parsecs) rippling can also be seen (Raymond et al. 2007; Winkler et al. 2014). Tycho’s remnant has a radius of about 3 pc, and its whole  $\text{H}\alpha$  shape is no longer circular (Raymond et al. 2010). Indeed, several observational results have indicated the inhomogeneity of the ambient medium around SN 1006 (Dubner et al. 2002; Raymond et al. 2007; Miceli et al. 2014) and Tycho’s remnant (Reynoso et al. 1991; Ishihara et al. 2010). SNR 0509–67.5 is also round in shape with a radius of 3.6 pc, however, the southwest part of

the remnant is rippled and has many  $\text{H}\alpha$  filaments (see, e.g., Figure 1 of Helder et al. 2010). These observational results for  $\text{H}\alpha$  morphology on a few parsecs or smaller scale are consistent with our model with a typical ISM density fluctuation. Therefore, we should still pay attention to the effect of upstream inhomogeneity when the CR acceleration efficiency is discussed in these remnants. In order to reproduce the morphology of the whole remnant and the smaller-scale structure simultaneously, we require larger-scale simulation, keeping the same spatial resolution as in the present study, which is currently difficult due to the limitation of computer resources and must remain for a future work.

At oblique shocks, the upstream velocity component parallel to the shock front is not dissipated across the shock. For the case of an edge-on view of the rippled shock, such a component mainly turns out to be transverse to the LOS in the downstream region (see Figure 1(a)), so that it becomes an unseen, missing component—it does not even contribute to the width of the broad  $\text{H}\alpha$  line. In previous observational arguments, the missing energy was attributed to CR acceleration. In the present case, the post-shock fluid stream lines become “turbulence” after the crossing time of the shock rippling scale (the driving scale of “turbulence”). Note that this driving scale  $\sim 0.1$  pc (Inoue et al. 2013) is much larger than the typical width of the emission region, indicating that turbulent line broadening cannot be measured by  $\text{H}\alpha$  emission. Since the downstream turbulence is created by the effect of the rippled shock wave (Giacalone & Jokipii 2007), the induction of the turbulence can be understood as a consequence of Crocco’s theorem in hydrodynamics. The strength of the induced turbulence depends on the degree of the density inhomogeneity in the preshock medium. In Inoue et al. (2013), we found that the velocity dispersion of the turbulence can be well described by a formula obtained from the modified growth velocity of the Richtmyer–Meshkov instability as a function of the upstream density dispersion.

One can also find from the synthetic  $\text{H}\alpha$  image (bottom panel of Figure 2) that regions 1–6 precede regions 9–12, so that one might think that the proper motion velocities of regions 1–6 are higher than those of regions 9–12. However, this is not true (see Table 1). We find the outermost parts of the  $\text{H}\alpha$  filament do not always have the fastest shock velocity or the highest downstream temperature. This is because the shock front has effective surface tension and is stable with respect to the rippling deformations. Thus, even though some regions of the shock front are decelerated (accelerated) due to the passage of the dense (thin) region, they will be accelerated (decelerated) once the dense (thin) region passes into the downstream region.

In the present analysis, we have seen  $\eta \geq 0$  (that is,  $T_{\text{proper}} > T_{\text{down}}$ ) for all 16 regions, which implies that the proper motion velocity  $V_{\text{proper}}$  is larger than the velocity component normal to the shock surface  $V_n$ . We have set our LOS orthogonal to the global direction of the shock propagation. However, when the shock wave propagates nearly toward us (along the LOS),  $V_{\text{proper}}$  can be smaller than  $V_n$ . For example, Salvesen et al. (2009) measured the proper motion velocity of  $\text{H}\alpha$  filaments of the Cygnus Loop and simultaneously derived the downstream gas temperature from the thermal X-ray spectrum there. Then, they obtained the fraction of the CR pressure  $P_{\text{CR}}$  to the thermal gas pressure  $P_{\text{G}}$  in the downstream

region. According to their analysis, many  $H\alpha$  filaments have  $P_{\text{CR}}/R_G \leq 0$ . Since they assumed a strong shock with a compression ratio of 4, an adiabatic index of  $5/3$ , and a temperature equilibrium of  $T_e = T_i = T_{\text{down}}$ , the ratio  $P_{\text{CR}}/R_G$  is related to  $\eta$  as

$$\frac{P_{\text{CR}}}{R_G} = \frac{\eta}{1 - \eta}. \quad (9)$$

Here  $T_e$  and  $T_i$  are downstream electron and ion temperatures, respectively. Since  $\eta > 1$  is unphysical,  $P_{\text{CR}}/R_G < 0$  means  $\eta < 0$ , that is,  $T_{\text{proper}} < T_{\text{down}}$ . Therefore, the observational result for the Cygnus Loop might be explained by our model. Moreover, it is suggested that the proper motion velocity is underestimated due to the shock obliqueness.

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#### APPENDIX ANALYTICAL ESTIMATE OF $\eta$

We present a simple analytical argument which relates  $\eta$  to the upstream density fluctuation. We simplify the upstream medium as a mixture of two components: overdense clumps with density  $\langle \rho \rangle_0 + \Delta\rho$  and underdense gas with density  $\langle \rho \rangle_0 - \Delta\rho$ . The characteristic size of the clumps  $\lambda$  is the same as their separation. In the present case,  $\lambda$  is on the order of  $L_{\text{box}} = 2$  pc. Initially, the planar shock surface collides with the clumps. Its propagation speed in the clumps  $V_+$  is slower than that in the underdense gas  $V_-$ , so that the shock surface is deformed. Assuming momentum conservation, these are related as

$$(\langle \rho \rangle_0 + \Delta\rho)V_+^2 \approx (\langle \rho \rangle_0 - \Delta\rho)V_-^2. \quad (\text{A1})$$

Then, we find  $V_+/V_- \approx 1 - \Delta\rho/\langle \rho \rangle_0$  for small  $\Delta\rho/\langle \rho \rangle_0$ . As the shock front goes ahead a distance  $\lambda$  in the underdense gas, the shock surface in the clumps is left at a distance  $\delta = \lambda - (\lambda/V_-)V_+$  behind the preceding surface in the underdense gas. Therefore, one derives the deformation angle  $\theta$ , which is an angle between the shock velocity  $V_{\text{sh}}$  and the shock normal (see Figure 1(b)), as  $\theta \approx \delta/\lambda \approx \Delta\rho/\langle \rho \rangle_0$ .

The downstream temperature  $T_{\text{down}}$  is predominantly determined by the overdense clump, that is, Equation (2) with  $V_n = V_+ \cos \theta$ . For our present geometry, in which shock surfaces are viewed nearly edge-on, the proper motion velocity  $V_{\text{proper}}$  is roughly equal to the shock velocity  $V_{\text{sh}}$ . If we observe the proper motion velocity of the shock surface propagating into the overdense clump, then  $V_{\text{proper}} \approx V_+$ , while  $V_{\text{proper}} \approx V_-$

for the shock propagation into the underdense gas. Hence, we find  $\eta = 1 - \cos^2 \theta \approx (\Delta\rho/\langle \rho \rangle_0)^2$  for the former case and  $\eta = 1 - (V_+/V_-)^2 \cos^2 \theta \approx 2\Delta\rho/\langle \rho \rangle_0$  for the latter case. In a more complicated case of our present simulation study, we expect  $V_+ \lesssim V_{\text{sh}} \lesssim V_-$  and these values of  $\eta$  may give lower and upper bounds, so that  $(\Delta\rho/\langle \rho \rangle_0)^2 \lesssim \eta \lesssim 2\Delta\rho/\langle \rho \rangle_0$ .

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