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Proto-magnetar jets as central engines for broad-lined Type Ic supernovae

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ABSTRACT

A subset of Type Ic supernovae (SNe Ic), broad-lined SNe Ic (SNe Ic-bl), show unusually high kinetic energies (∼10^{52} \text{erg}) that cannot be explained by the energy supplied by neutrinos alone. Many SNe Ic-bl have been observed in coincidence with long gamma-ray bursts (GRBs) that suggests a connection between SNe and GRBs. A small fraction of core-collapse supernovae form a rapidly rotating and strongly magnetized protoneutron star (PNS), a proto-magnetar. Jets from such magnetars can provide the high kinetic energies observed in SNe Ic-bl and also provide the connection to GRBs. In this work, we use the jetted outflow produced in a 3D general relativistic magnetohydrodynamic CCSN simulation from a consistently formed proto-magnetar as the central engine for full-star explosion simulations. We extract a range of central engine parameters and find that the extracted engine energy is in the range of 6.231 × 10^{51}−1.725 × 10^{52} \text{erg}, the engine time-scale in the range of 0.479−1.159 s and the engine half-opening angle in the range of ∼9°−19°. Using these as central engines, we perform 2D special relativistic (SR) hydrodynamic (HD) and radiation transfer simulations to calculate the corresponding light curves and spectra. We find that these central engine parameters successfully produce SNe Ic-bl that demonstrates that jets from proto-magnetars can be viable engines for SNe Ic-bl. We also find that only the central engines with smaller opening angles (∼11°) form a GRB implying that GRB formation is likely associated with narrower jet outflows and Ic-bl’s without GRBs may be associated with wider outflows.

Key words: MHD – gamma-ray burst: general – stars: general – stars: jets – stars: magnetars – supernovae: general

1 INTRODUCTION

Gamma-ray bursts (GRBs) are short and intense flashes of gamma rays at cosmological distances (e.g. Fishman & Meegan 1995). They can be classified as short GRBs and long GRBs, depending on the duration of the burst. Core-collapse supernovae (CCSNe) are explosions of massive stars at the end of their lifetime, forming a neutron star or a black hole in the process (e.g. Woosley & Janka 2003). The connection between SNe and GRBs has been theorized before (Colgate 1968; Woosley 1993; Paczyński 1998) but was only confirmed observationally with the discovery of SN 1998bw coincident with GRB 980425 (Galama et al. 1998), which suggested a connection between two phenomena. The SN–GRB connection has since become firmer with the nearly simultaneous discovery of SN2003dh with GRB 030329 (Hjorth et al. 2003; Matheson et al. 2003; Stanek et al. 2003) and is now well established with additional observations, e.g. SN 2006aj/GRB 060218 (Campana et al. 2006; Modjaz et al. 2006; Pian et al. 2006; Sollerman et al. 2006), and SN 2010bh/GRB 100316D (Chornock et al. 2010; Starling et al. 2011).

All SNe that have been linked to GRBs belong to the class of broad-lined Type Ic supernovae (SNe Ic-bl; e.g. Woosley & Bloom 2006; Modjaz 2011; Hjorth & Bloom 2012; Cano et al. 2017). SNe Ic-bl have broad spectral lines indicating high photospheric velocities (∼15 000−30 000 km s^{-1}; Modjaz et al. 2016) and high kinetic energies (∼10^{52} \text{erg}; e.g. Iwamoto et al. 1998; Oli vera E. et al. 2012). Their optical spectra show no H or He. The extreme kinetic energies involved in SNe Ic-bl challenge the underlying standard explosion mechanism because the energy supplied by neutrinos is not sufficient to explain the high kinetic energies observed (e.g. Burrows & Vartanyan 2021). Jets from rapidly rotating protoneutron stars (PNSs) formed in CCSNe explosions can provide the high kinetic energies observed in SNe Ic-bl and also provide the connection to GRBs (Komissarov 2008; Metzger et al. 2011; Wang et al. 2016; Sobacchi et al. 2017; Burrows & Vartanyan 2021). However, whether a single jet engine can explain both SNe Ic-bl and GRBs is still unclear. Many SNe Ic-bl have been observed without an accompanying GRB, which raises the question whether GRBs are present in all SNe Ic-bl. Modjaz et al. (2016) found in a statistical study that SNe with an accompanying GRB have broader spectra compared to SNe without an observed GRB and that line-of-sight effects alone are not likely to explain the fraction of SNe Ic-bl with and without accompanying GRBs.

Some CCSNe explosions can lead to the formation of a rapidly rotating PNS where vigorous convection coupled with rapid rotation forms very strong magnetic fields (∼10^{15} \text{G}) due to magnetic field amplification via dynamo action (Duncan & Thompson 1992). Simulations show that the spin-down of the rapidly rotating PNS can...
supply energy to the jet outflow resulting in higher kinetic energies compared to a neutrino-driven SN explosion (Burrows et al. 2007; Mazzali et al. 2014). In principle, the SN explosion energy and light curves derived from CCSNe can be tested with self-consistent MHD simulations following the jet all the way to breakout of the stellar surface. However, this is currently numerically infeasible in multiple dimensions because of the difference in length-scales of the PNS (∼10 km) and the progenitor star (∼10^6 km), as well as the difference in time-scales of jet formation (∼0.1 s) and jet breakout (∼10 s), which need to be resolved numerically leading to a spatial resolution of ∼0.1 km and a corresponding time-step of ∼10^-7 s. The current approach for full-star simulations is to excise some portion (∼1000 km) from the centre of the star and assume a hypothetical engine injecting energy into the rest of the star. This is known as the central engine paradigm (e.g. Suzuki 2019).

Under the central engine paradigm, Barnes et al. (2018; B2018, hereafter) combined hydrodynamics and radiation-transfer simulations end-to-end to simulate a GRB jet-driven SN Ic-bl. The success of this numerical set-up depends on its ability to produce high kinetic energies and broad spectral features typical of SNe Ic-bl. For a presumed set of engine parameters, B2018 were successful in producing a SN Ic-bl that was roughly consistent with observations. In their work, they chose values for the central engine parameters consistent with observations. Whether such engine parameters are possible from PNS formation in CCSNe simulations remains to be investigated. We probe this in this work.

In this work, we use the data from a 3D magnetorotational CCSN simulation (Moesta et al. 2014) to estimate the engine parameters. We then use these parameters to perform hydrodynamic and radiation-transfer calculations. We closely follow the numerical set-up of B2018 for the hydrodynamics and radiation transfer simulations. This is the first study to carry out an end-to-end CCSN simulation, hydrodynamics, and radiation transfer calculation in multiple dimensions. We find that the central engine parameters extracted from jet outflows of 3D CCSN simulation successfully produce a SN Ic-bl. This demonstrates that jets from PNS formation can be a viable engine for SN Ic-bl.

In Section 2, we describe the tools used in our numerical set-up. In Section 3, we present the methodology and results for parameters extracted from the 3D CCSN simulation, as well as the results for SN observables. We discuss the obtained results in Section 4.

2 NUMERICAL SET-UP

We combine the results from a 3D magnetorotational CCSN simulation with a suite of advanced numerical codes to model a jet-driven SN explosion and its emergent light curves and spectra. We use the 3D CCSN simulation of Moesta et al. (2014) to estimate the engine parameters. We perform the hydrodynamic simulations with the 2D special relativistic jet code (SR) JET code and carry out radiation transport with SEDONA to generate the light curves and spectra. JET takes as input the extracted engine parameters and gives as output the density, temperature and 56Ni mass distribution. We then use these as input to SEDONA to generate light curves and spectra. This numerical set-up allows us to study a jet-driven SN explosion of the star, including the physics of core collapse, in multiple dimensions.

2.1.1 3D GRMHD CCSN simulation for central engine parameter estimation

Moesta et al. (2014) perform 3D general relativistic magnetohydrodynamic (GRMHD) simulations of rapidly rotating strongly magnetized CCSNe. The simulation was performed in ideal GRMHD with the EINSTEIN TOOLKIT (Löffler et al. 2012; Mösta et al. 2014). They employ a finite-temperature microphysical equation of state (EOS), using the 10 = 220 MeV variant of EOS of Lattimer & Swesty (1991), and an approximate treatment of neutrino transport (O’Connor & Ott 2010; Ott et al. 2012). They use the 25 M⊙ presupernova model E25 (Heger, Langer & Woosley 2000) as the progenitor. They perform the simulations in full unconstrained 3D as well as those constrained to 2D, both of which start from identical initial conditions. They find that 2D and 3D simulations show fundamentally different evolutions. A strong jet-driven explosion is obtained in 2D. In contrast, the jet disrupts in full 3D and results instead in a broad lobar outflow. In this work, we use the results of the 3D simulation and estimate the central engine parameters from the lobar outflow.

2.1.2 Hydrodynamics using JET

JET (Duffell & MacFadyen 2013) is a variant of TESS (Duffell & MacFadyen 2011), with a specific application to radial outflows. JET uses a mesh that moves outward radially, thus making it effectively Lagrangian in radial direction and able to accurately evolve flows over large dynamic length-scales. This is very useful in this work because we need to evolve the flow from ∼10^3 to ∼10^4 km. We have used the most recent version of JET code for our hydrodynamics calculations. Except for varying the central engine parameters, we keep other simulation parameters as in B2018.

Radioactive decay of 56Ni is the source of luminosity for the SN, but JET does not include a nuclear reaction network to accurately model the synthesis of 56Ni during the hydrodynamic phase. B2018 provide a detailed description of 56Ni synthesis in the JET code, but we briefly reiterate it here because it is fundamental to the SN model. JET uses an approximate treatment to estimate 56Ni production using a simple temperature condition in which any zone where temperature exceeds a certain temperature, T_{max}, is assumed to burn to pure 56Ni. We use T_{max} = 5 × 10^9 K as in B2018. We have not included gravity in the JET simulations (as in B2018). The treatment of gravity will affect the velocities of any marginally bound material, but the typical escape velocity for the adopted progenitor star is ∼0.002 c. This is much smaller than the typical velocity of ejected material in the explosion and this makes the effect of gravity negligible in this case.

2.1.3 Radiation transport using SEDONA

SEDONA is a 3D time-dependent multi-wavelength radiative transport code based on Monte Carlo techniques, which can be used to calculate SN observables from the hydrodynamic variables of an SN (Kasen, Thomas & Nugent 2006). SEDONA self-consistently solves the temperature structure of the ejecta and generates the temperature and composition dependent opacities required for photon transport. Our calculation assumes the ejecta is in local thermodynamic equilibrium (LTE). The code calculates the light curves and spectra. It outputs the supernova’s full spectral time-series, thus providing a link between the hydrodynamic calculation and SN observables. We have used the most recent version of SEDONA in a 2D axisymmetric setting. Our numerical set-up for SEDONA calculations is the same as that of B2018.

2.1.4 Progenitor and jet engine models

We use the same progenitor and engine models as B2018. A detailed description of the progenitor and engine models can be found there.
Table 1. Progenitor composition.

<table>
<thead>
<tr>
<th>Element</th>
<th>He</th>
<th>C</th>
<th>N</th>
<th>O</th>
<th>Ne</th>
<th>Mg</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td>6.79e−3</td>
<td>2.27e−2</td>
<td>2.91e−5</td>
<td>9.05e−1</td>
<td>1.37e−2</td>
<td>8.46e−3</td>
</tr>
<tr>
<td>Si</td>
<td>2.69 −2</td>
<td>1.04e−2</td>
<td>1.60e−3</td>
<td>6.63e−4</td>
<td>5.11e−7</td>
<td>3.50e−3</td>
</tr>
</tbody>
</table>

but we briefly reiterate the relevant details here. The progenitor consists of an analytic model that reasonably approximates the major features of a stripped-envelope Wolf–Rayet star having zero-age main-sequence mass of 40 M⊙ and solar metallicity. We excise the material interior to 1.5 × 10−3 R⊙ (∼1000 km) of the star and set the density in the cavity to 10−3 times the density at the cavity boundary. The density exterior to the cavity is given by

\[ \rho_{\text{init}}(r) = \frac{0.0615 M_0}{R_0^3} \left(\frac{R_0}{r}\right)^{2.65} \left(1 - \frac{r}{R_0}\right)^{2.5}, \]

where \( R_0 = 1.6 R_⊙ \) is the radius of the star and \( M_0 = 2.5 M_⊙ \) is the mass of the material outside the cavity. The composition of the progenitor in terms of mass fractions of various elements is shown in Table 1.

The engine is defined by the total energy injected, \( E_{\text{eng}} \), the engine half-opening angle, \( \theta_{\text{eng}} \); and the characteristic time-scale of the engine, \( t_{\text{eng}} \). We taper off the engine exponentially as

\[ L_{\text{eng}}(t) = \frac{E_{\text{eng}}}{t_{\text{eng}}} \times \exp \left[-t/t_{\text{eng}}\right]. \]

We estimate the values of \( E_{\text{eng}}, \theta_{\text{eng}}, \) and \( t_{\text{eng}} \) using the 3D CCSN simulation from Moesta et al. (2014). The values of a few important JET and SEDONA parameters used in our numerical setup are listed in Table 2.

2.1.5 Reproduction of earlier results

B2018 have already performed an end-to-end hydrodynamic and radiation-transfer simulation with a presumed set of engine parameters. In this work, we add to this set-up the engine parameters extracted from a 3D CCSN simulation, instead of using a presumed set of parameters. We note that we are not performing a true transition from the 3D GRMHD CCSN simulation to the JET simulations in this work but are obtaining engine energy, time-scale and half-opening angle from the 3D GRMHD CCSN simulation and providing it as an input to the JET simulations via the parametrized engine model previously described in this section. We keep all other engine parameters same as in B2018. We have used the most recent versions of JET and SEDONA for this work. To validate our methodology and isolate the effects of changes to JET and SEDONA on simulation outputs, we first reproduce the results of B2018 using our updated computational suite. We find that our model spectra show no significant differences from the results of B2018. Our spectra have fairly broad lines representative of SNe Ic-bl, with enhanced broadening and blue-shifting for polar viewing angles at times less than \( t_{\text{peak}} \).

3 RESULTS

3.1 Extraction of engine parameters

Next, we extract from the CCSN simulation an effective engine time-scale, energy, and half-opening angle for use in new simulations with JET. The PNS formed in the 3D CCSN simulation produces a wide-lobed outflow as the actual jet gets disrupted by an \( m = 1 \) kink instability. It is this outflow that provides the energy for exploding the stellar material as a SN. We use this outflow to estimate the total energy, the half-opening angle, and the characteristic time-scale of the central engine. Data for various physical parameters in the 3D CCSN simulation is available up to \( ∼130 \) ms after bounce. However, this time-scale is much smaller than the time-scale involved in central engine and stellar SN dynamics. We therefore need to extrapolate the available data in order to get an estimate for the engine parameters. We use the spin-down rate of the PNS to estimate the time-scale of the central engine and we assume that the spin-down rate remains constant for \( ∼1 \) s after data availability. In reality, the accretion rate may deviate from the extrapolated behaviour at late times (\( t > 0.5 \) s; see Burrows et al. 2020). This could lead to a different engine behaviour at late times, which could lead to a different \( t_{\text{eng}} \).

3.1.1 Estimation of total energy and characteristic time-scale

The jet produced in the 3D CCSN simulation gets disrupted and a wide-lobed outflow of material forms instead. We need to estimate the central engine total energy from this resultant flow pattern. For that we identify the material that is gravitationally unbound from the newly formed PNS and can be considered ejected from it. It is this unbound material that provides the energy required for the explosion of the star. We define a fluid element to be unbound if it satisfies the Bernoulli criterion, i.e., \( bu < −1 \) (e.g. Kastaun & Galeazzi 2015), where \( b \) is the fluid specific enthalpy and \( u \) is the covariant time component of the fluid element 4-velocity.

We obtain the energy of the outflow as a function of time for the available data. The energy of the outflow is comprised of kinetic and

Table 2. A few important JET and SEDONA parameters.

<table>
<thead>
<tr>
<th>Parameter</th>
<th>JET</th>
<th>Value</th>
<th>Parameter</th>
<th>SEDONA</th>
<th>Value</th>
</tr>
</thead>
<tbody>
<tr>
<td>Adiabatic index</td>
<td>4/3</td>
<td></td>
<td>Number of particles</td>
<td></td>
<td>2 × 10^5</td>
</tr>
<tr>
<td>Injected Lorentz factor</td>
<td>50</td>
<td></td>
<td>Number of viewing bins</td>
<td></td>
<td>9 (between 0 and π)</td>
</tr>
<tr>
<td>Energy-to-mass ratio</td>
<td>1000</td>
<td></td>
<td>Transport frequency grid (Logarithmic)</td>
<td></td>
<td>{2.7 × 10^{13}, 2 × 10^{14}, 0.0006}</td>
</tr>
<tr>
<td>Nozzle size</td>
<td>~6000 km</td>
<td></td>
<td>Spectrum frequency grid (Logarithmic)</td>
<td></td>
<td>{3.0 × 10^{13}, 2 × 10^{14}, 0.005}</td>
</tr>
<tr>
<td>Initial number of radial bins</td>
<td>512</td>
<td></td>
<td>Start time</td>
<td></td>
<td>0.5 d</td>
</tr>
<tr>
<td>Number of angular bins</td>
<td>256 (between 0 and π/2)</td>
<td></td>
<td>Stop time</td>
<td></td>
<td>80.0 d</td>
</tr>
<tr>
<td>Maximum value of a time-step</td>
<td></td>
<td></td>
<td>Number of velocity bins</td>
<td></td>
<td>0.1 d</td>
</tr>
<tr>
<td>Number of velocity bins</td>
<td></td>
<td></td>
<td></td>
<td></td>
<td>100 (between 0 and 0.2c)</td>
</tr>
</tbody>
</table>

Note: a frequency grid = \{\nu_{\text{start}}(s^{-1}), \nu_{\text{stop}}(s^{-1}), Δ\}, dν = νΔ.
internal energy of fluid elements, as well as the energy due to the magnetic field. We assume that only the unbound material forms a part of the outflow and thus do not consider bound material for the energy calculation. The time variation of the energy of outflow is shown in Fig. 1. We find that the energy increases slowly at first, but shows a steady linear increase after $\sim 110$ ms post-bounce, the time at which an outflow along the rotation axis is launched. We use the energy evolution after this time for extrapolation.

We also calculate the rotational energy of the PNS as a function of time. The rotational energy of the newly formed PNS is affected by the infalling stellar material as well as the outflow of material from the core. The infalling material imparts angular momentum and thus tends to increase the rotational energy, whereas the material in the outflow tends to decrease the rotational energy. We plot the time dependence of the rotational energy of the material within a certain radius becomes zero. We show $t_{\text{eng}}$ as a function of radius in the figure. $t_{\text{eng}}$ peaks at the radius of 50 km and converges for larger radii. We choose the value of $t_{\text{eng}}$ at peak (1159 ms) and convergence ($\sim 479$ ms) as the two limiting cases for further investigation.

We fit the rotational energy in the 3D CCSN simulation after $\sim 110$ ms post-bounce with a straight line. In order to get a limiting case, we calculate the time at which this straight line fit leads to zero rotational energy. We use this time as the characteristic time-scale ($t_{\text{eng}}$) of the central engine. We use $t_{\text{eng}}$ to extrapolate the linear part
Table 3. Extracted values of characteristic time-scale and total energy of the central engine.

<table>
<thead>
<tr>
<th>Radius (km)</th>
<th>Characteristic time-scale $t_{\text{eng}}$ (s)</th>
<th>Total engine energy $E_{\text{eng}}$ (erg)</th>
</tr>
</thead>
<tbody>
<tr>
<td>50</td>
<td>1.159</td>
<td>$1.725 \times 10^{52}$</td>
</tr>
<tr>
<td>~130</td>
<td>0.479</td>
<td>$6.231 \times 10^{51}$</td>
</tr>
</tbody>
</table>

Figure 5. Panel (a) shows $\beta = P_{\text{gas}}/P_{\text{mag}}$ in the $x$-$z$ plane ($y = 0$) in Cartesian coordinates at $\sim 110$ ms post-bounce. The PNS is located at the origin. The 3D data in Cartesian coordinates ($x, y, z$) is converted to Cylindrical coordinates ($\rho, \phi, z$). Panel (b) shows the data in cylindrical coordinates in the $\rho$-$z$ plane ($\phi = 0$). Only those points are selected which are unbound, have positive outward $z$-velocity and have $\beta = 0.1 \pm 0.005$. The selected points are fit with a straight line to obtain the effective opening angles ($\theta_{\text{up}}, \theta_{\text{down}}$) for this $\phi$-slice ($\phi = 0$). The averaging of these angles for all $\phi$-slices gives the effective opening angle $\theta_{\text{avg}}(t)$ for this time-step.

Figure 6. $\theta_{\text{avg}}$ as a function of time for $\beta = 0.1, 0.2, \text{and } 0.3$. The opening angles become larger for higher values of $\beta$ because higher $\beta$ corresponds to less magnetized fluid elements, thus farther away from the jet axis. We consider $\beta = 0.1$ and 0.3 for central engine parameter estimation to test dependence on $\beta$.

of outflow energy assuming that the outflow energy variation remains linear up to $t_{\text{eng}}$. The extrapolated outflow energy value at $t_{\text{eng}}$ gives the total energy of the central engine. We demonstrate this method in Fig. 3. It should be noted that the total rotational energy initially cannot be assumed to be the total energy of the central engine because accretion of material into the vicinity of the PNS adds energy to the engine over time.

Since we are extrapolating the rotational energy to calculate $t_{\text{eng}}$, it is important that we consider the possible parameter dependence of $t_{\text{eng}}$. To do so, we vary the radius within which material is considered for the rotational energy calculation. We vary the radius from 20 to 150 km. For each radius, we fit the rotational energy after $\sim 110$ ms post-bounce with a straight line and calculate $t_{\text{eng}}$ by extrapolating this straight line fit to zero rotational energy. We show $t_{\text{eng}}$ as a function of radius in Fig. 4. We find that $t_{\text{eng}}$ has a peak at $\sim 1159$ ms, and it converges to $\sim 479$ ms for larger radii. We therefore explore $t_{\text{eng}} = 1159$ ms and $t_{\text{eng}} = 479$ ms as limiting cases for this work. Extrapolating the linear part of the outflow energy (after $\sim 110$ ms post-bounce) to these characteristic time-scales gives an engine energy of $1.725 \times 10^{52}$ erg for $t_{\text{eng}} = 1159$ ms and $6.231 \times 10^{51}$ erg for $t_{\text{eng}} = 479$ ms. We present these parameters in Table 3.

3.1.2 Estimation of the half-opening angle

To estimate the half-opening angle of the central engine from the wide-lobed outflow of the PNS, we use the fluid elements that are highly magnetized. We use the plasma $\beta$ parameter, defined as $\beta = P_{\text{gas}}/P_{\text{mag}}$. For highly magnetized material, $\beta \ll 1$. The jet consists of highly magnetized material and we choose two separate cases to identify the material in the jet for the calculation of the opening angle: $\beta \sim 0.1$ and $\beta \sim 0.3$. We do this because the boundary of the jet is not precisely defined and there is not a single fixed value of $\beta$ that we can use to identify the jet boundary. These two choices of $\beta$ allow us to explore a wider range of opening angles for their ability to produce SNe Ic-bl. In addition, we only consider unbound fluid elements using the Bernoulli criterion.
Fluid elements with a straight line passing through the PNS surface (Fig. 7). Extraction of regions: up ($\theta_{\text{up}}$, $\phi_{\text{up}}$) and down ($\theta_{\text{down}}$, $\phi_{\text{down}}$) for $\beta = 0.1$ and $0.3$. We consider two cases for extraction of $\theta_{\text{avg}}$ for each $\beta$: (i) $\theta_{\text{avg}}(t) = 0.5(t \theta_{\text{up}}(t) + \theta_{\text{down}}(t))$ and (ii) $\theta_{\text{avg}} = \sin(\omega t + \delta)$. Case (i) gives a constant $\theta_{\text{avg}}$, while case (ii) gives a time variable $\theta_{\text{avg}}$.

Data from the 3D CCSN simulation is available in Cartesian coordinates ($x$, $y$, $z$) where $z$ is the axis of rotation of the PNS. We convert this data to cylindrical coordinates ($\rho$, $\phi$, $z$) so that averaging the obtained angles in the azimuthal direction becomes convenient. For a given time-step, at a given $\phi$-slice, we locate the fluid elements that are unbound, have positive outward $z$-velocity and have $\beta = 0.1(0.3) \pm 0.005$. We separate these points in two regions: up ($z > 0$) and down ($z < 0$), and find the angles for these two regions separately. For each region, we fit the selected fluid elements with a straight line passing through the PNS surface ($\sim 15$ km). We determine the angle of this line with the $z$-axis as $\theta_{\text{up}}(\phi, t)$ for $z > 0$ and $\theta_{\text{down}}(\phi, t)$ for $z < 0$. We demonstrate the calculation of $\theta_{\text{up}}$ and $\theta_{\text{down}}$ at $t \sim 110$ ms post-bounce for $\phi = 0$ in Fig. 5. We average $\theta_{\text{up}}$ and $\theta_{\text{down}}$ over all values of $\phi$ to get $\theta_{\text{up,avg}}(t)$ and $\theta_{\text{down,avg}}(t)$, respectively. We calculate the average half-opening angle for the entire time-step as $\theta_{\text{avg}}(t) = \frac{1}{2} [\theta_{\text{up,avg}}(t) + \theta_{\text{down,avg}}(t)]$. This azimuthal averaging of angles minimizes the differences due to any possible small tilt of rotation axis with the $z$-axis and thus gives us an effective half-opening angle.

We calculate $\theta_{\text{avg}}$ for all values of $t$ where it is feasible, which comes out to be $105 \leq t - t_b \leq 130$ ms for $\beta = 0.1$, and $86 \leq t - t_b \leq 130$ ms for $\beta = 0.3$. For times earlier than 105(86) ms, the magnetic fields in the not yet fully formed outflow are not strong enough to produce $\beta$ as low as 0.1(0.3) for all $\phi$-slices. We show the time dependence of $\theta_{\text{avg}}$ for $\beta = 0.1, 0.2, \text{and } 0.3$ in Fig. 6. We perform the remaining analysis only for $\beta = 0.1$ and $\beta = 0.3$ as we are interested in the limiting values of the possible opening angle. We find that $\theta_{\text{avg}}$ varies from $\sim 9(14^\circ)$ to $\sim 13(19^\circ)$ for $\beta = 0.1(0.3)$. In order to get the half-opening angle of the central engine from this data, we take two cases. In the first case we take the average over time for $\theta_{\text{avg}}(t)$. As the outflow in the 3D simulation effectively precesses in time due to the kink instability, we try to parametrize this via a sinusoidal varying in time. In this second case we fit $\theta_{\text{avg}}$ as $\theta(t) = A \sin(\omega t + \delta) + \beta$. We show the data points as well as the best fit in Fig. 7. We summarize the extracted opening angles for all cases in Table 4.

### 3.1.3 Summary of parametric central engine models

We have extracted two different values of ($E_{\text{eng}}$, $t_{\text{eng}}$), as summarized in Table 3. For $\theta_{\text{avg}}$, we extracted four different values: two constant in time and two varying in time, as summarized in Table 4. We combine these parameters and construct eight parametric models for the central engine. They are summarized in Table 5. Model 1 is the reproduction of the work of B2018. We find that the extracted parameters in model 2 are very close to the values used by B2018. Model 2 consists of ($E_{\text{eng}}$, $t_{\text{eng}}$) extracted from peak $t_{\text{eng}}$, and $\theta_{\text{avg}}$ extracted from time-averaged $\theta_{\text{avg}}(t)$ for $\beta \sim 0.1$. We perform

![Figure 7](https://example.com/image7.png)

**Table 4.** Extracted values of opening angles of the central engine.

<table>
<thead>
<tr>
<th>$\beta$</th>
<th>Time averaged $\theta_{\text{avg}}(t)$:</th>
<th>Sinusoidal fit of $\theta_{\text{avg}}(t)$:</th>
</tr>
</thead>
<tbody>
<tr>
<td>0.1</td>
<td>$10.63 \deg$</td>
<td>$11.60 + 2.25 \sin(\omega t + \delta_1)$</td>
</tr>
<tr>
<td></td>
<td>$T_1 = 2\pi/\omega_1 = 51.4 , \text{ms, } \delta_1 = 3.72$</td>
<td></td>
</tr>
<tr>
<td>0.3</td>
<td>$17.50 \deg$</td>
<td>$15.49 + 3.95 \sin(\omega t + \delta_2)$</td>
</tr>
<tr>
<td></td>
<td>$T_2 = 2\pi/\omega_2 = 98.4 , \text{ms, } \delta_2 = 0.26$</td>
<td></td>
</tr>
</tbody>
</table>

**Table 5.** Central engine models constructed from the extracted parameters presented in Table 3 and 4.

<table>
<thead>
<tr>
<th>Engine model</th>
<th>$t_{\text{eng}}(\text{s})$</th>
<th>$E_{\text{eng}}(\text{erg})$</th>
<th>$\theta_{\text{eng}}(\deg)$</th>
</tr>
</thead>
<tbody>
<tr>
<td>Model 1</td>
<td>1.1</td>
<td>$1.8 \times 10^{52}$</td>
<td>11.5</td>
</tr>
<tr>
<td>Model 2</td>
<td>1.159</td>
<td>$1.725 \times 10^{52}$</td>
<td>10.63</td>
</tr>
<tr>
<td>Model 3</td>
<td>1.159</td>
<td>$1.725 \times 10^{52}$</td>
<td>17.50</td>
</tr>
<tr>
<td>Model 4</td>
<td>0.479</td>
<td>$6.231 \times 10^{51}$</td>
<td>10.63</td>
</tr>
<tr>
<td>Model 5</td>
<td>0.479</td>
<td>$6.231 \times 10^{51}$</td>
<td>17.50</td>
</tr>
<tr>
<td>Model 6</td>
<td>1.159</td>
<td>$1.725 \times 10^{52}$</td>
<td>11.60 $+ 2.25 \sin(\omega t + \delta_1)$</td>
</tr>
<tr>
<td>Model 7</td>
<td>1.159</td>
<td>$1.725 \times 10^{52}$</td>
<td>15.49 $+ 3.95 \sin(\omega t + \delta_2)$</td>
</tr>
<tr>
<td>Model 8</td>
<td>0.479</td>
<td>$6.231 \times 10^{51}$</td>
<td>11.60 $+ 2.25 \sin(\omega t + \delta_1)$</td>
</tr>
<tr>
<td>Model 9</td>
<td>0.479</td>
<td>$6.231 \times 10^{51}$</td>
<td>15.49 $+ 3.95 \sin(\omega t + \delta_2)$</td>
</tr>
</tbody>
</table>
Figure 8. Mass density, $\rho$ (left-hand panel) and $^{56}$Ni mass fraction, $\chi$ (right-hand panel) at the end of the JET simulations ($t = 3733$ s) for models 2–9. We use these snapshots as the starting point for the SEDONA calculations. The white line shows $v = 0.2c$. 

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Figure 9. Bolometric light curves for our most realistic model (model 2, solid lines) along with the associated uncertainties from other models (shaded region), for polar and equatorial viewing angles. The rise times of the light curves are in the range of $\sim 10^{-18}$ d, while the peak bolometric luminosities lie in the range of $\sim 4 \times 10^{42} - 9 \times 10^{42}$ erg s$^{-1}$.

Figure 10. Peak luminosities ($L_{\text{peak}}$) and rise times ($t_{\text{peak}}$) of light-curves of various SNe Ic-bl/GRB-SNe reconstructed by Prentice et al. (2016) compared with the light curves of our models. The blue- and red-shaded regions show the bounds on the parameter space constrained by polar and equatorial light curves, respectively. The blue triangles show the angle average of polar and equatorial values of ($L_{\text{peak}}, t_{\text{peak}}$) for our different models. Our rise times are nearly consistent with observed SNe Ic-bl, while our peak luminosities span a subset of $L_{\text{peak}}$'s of observed SNe Ic-bl, but are well within the observational constraints.

3.2 Supernova observables

Using the central engine parameters described in Table 5, we perform hydrodynamic calculations using the JET code up to $t \sim 3700$ s. At this point, the flow becomes homologous and thus the outward velocity is proportional to the radius. We show the mass density (left-hand panel) and the $^{56}$Ni mass fraction (right-hand panel) at this time for models 2–9 in Fig. 8. At this time, the most relativistic material has reached a radius of $\sim 5 \times 10^{13} - 1 \times 10^{14}$ cm depending on the model. The SN ejecta is dominated by lower velocity material ($v \lesssim 0.2c$) that extends to $\sim 2 \times 10^{13}$ cm. We show this region in Fig. 8 and use it as the starting point for the SEDONA calculations. We find that the ejecta density structure shows some deviation from spherical symmetry in the form of lower density material in an approximately conical shape around the z-axis. For models 2, 4, 6, 8, and 9, the deviations from spherical symmetry are minor, with the angle of the cone $\lesssim 10^\circ$. Models 3, 5, and 7 show more deviation from spherical symmetry, with the angle of the cone $\lesssim 25^\circ$. More asymmetrical ejecta in models 3, 5, and 7 is due to the higher opening angle in these models ($\lesssim 17^\circ$). Model 9, despite having a higher opening angle, shows this behaviour to a lesser extent. The distribution of $^{56}$Ni shows much more anisotropy, with most of the $^{56}$Ni concentrated along the z-axis.

Table 6. SN and GRB properties of the various central engine models.

<table>
<thead>
<tr>
<th>Engine model</th>
<th>$t_{\text{peak}}$(d) (Eq, Po)</th>
<th>$L_{\text{peak}}$(erg s$^{-1}$) (Eq, Po)</th>
<th>$M(^{56}\text{Ni})/M_\odot$</th>
<th>Kinetic energy (erg)</th>
<th>Energy in $\gamma h \gtrsim 10$ (erg)</th>
<th>GRB present?</th>
</tr>
</thead>
<tbody>
<tr>
<td>Model 1</td>
<td>(15.3, 15.1)</td>
<td>(5.64, 4.92) $\times 10^{42}$</td>
<td>0.21</td>
<td>$4.72 \times 10^{51}$</td>
<td>$3.60 \times 10^{51}$</td>
<td>Yes</td>
</tr>
<tr>
<td>Model 2</td>
<td>(15.9, 15.9)</td>
<td>(4.78, 4.28) $\times 10^{42}$</td>
<td>0.18</td>
<td>$3.95 \times 10^{51}$</td>
<td>$4.08 \times 10^{51}$</td>
<td>Yes</td>
</tr>
<tr>
<td>Model 3</td>
<td>(11.7, 10.1)</td>
<td>(6.16, 9.24) $\times 10^{42}$</td>
<td>0.24</td>
<td>$9.58 \times 10^{51}$</td>
<td>0.0</td>
<td>No</td>
</tr>
<tr>
<td>Model 4</td>
<td>(17.7, 16.9)</td>
<td>(4.27, 3.78) $\times 10^{42}$</td>
<td>0.16</td>
<td>$3.72 \times 10^{51}$</td>
<td>$2.59 \times 10^{51}$</td>
<td>Yes</td>
</tr>
<tr>
<td>Model 5</td>
<td>(12.3, 11.1)</td>
<td>(6.40, 8.20) $\times 10^{42}$</td>
<td>0.24</td>
<td>$5.57 \times 10^{51}$</td>
<td>0.0</td>
<td>No</td>
</tr>
<tr>
<td>Model 6</td>
<td>(16.3, 15.3)</td>
<td>(6.39, 4.73) $\times 10^{42}$</td>
<td>0.20</td>
<td>$5.09 \times 10^{51}$</td>
<td>$1.21 \times 10^{50}$</td>
<td>Yes</td>
</tr>
<tr>
<td>Model 7</td>
<td>(14.1, 12.1)</td>
<td>(6.34, 6.93) $\times 10^{42}$</td>
<td>0.24</td>
<td>$7.34 \times 10^{51}$</td>
<td>$4.60 \times 10^{46}$</td>
<td>No</td>
</tr>
<tr>
<td>Model 8</td>
<td>(17.5, 16.7)</td>
<td>(4.82, 4.09) $\times 10^{42}$</td>
<td>0.18</td>
<td>$3.53 \times 10^{51}$</td>
<td>$2.45 \times 10^{50}$</td>
<td>Yes</td>
</tr>
<tr>
<td>Model 9</td>
<td>(15.5, 14.5)</td>
<td>(6.09, 5.76) $\times 10^{42}$</td>
<td>0.23</td>
<td>$5.17 \times 10^{51}$</td>
<td>0.0</td>
<td>No</td>
</tr>
</tbody>
</table>
We then perform the radiation transport calculations using SEDONA (starting at \( \sim 3700 \) s) in 2D cylindrical coordinates for the material within the region \( v_ρ, |v_z| \leq 0.2c \). We perform the SEDONA simulations using nine evenly spaced bins in \( \mu = \cos(\theta) \), \( \mu \in [1, 1] \), where \( \theta \) is the viewing angle with respect to the polar direction. The light curves and spectra that we show are averages within the bins.

As described in the previous section, model 2 is our most realistic central engine model extracted from the CCSN simulation. We explore models 3–9 to account for uncertainties around our most realistic model. We show the resulting light curves with respective uncertainties for polar and equatorial viewing directions in Fig. 9, where the solid lines indicate our most realistic model (model 2) and the shaded region indicates the uncertainties from the other models. We tabulate the properties of the associated SNe for all models in Table 6.

We find that the rise times of the bolometric light curves vary between \( \sim 10 \) and 18 d, while the peak luminosities vary between \( 4 \times 10^{42} \) and \( 9 \times 10^{42} \) erg s\(^{-1}\). Polar viewing angles show higher variation in peak luminosity (more than twice) compared to equatorial viewing angles. The viewing angle effect is small (\( \lesssim 2\)d) for the rise times of the different models. Prentice et al. (2016) reconstruct the pseudobolometric light curves of 85 stripped-envelope SNe from the available literature, out of which 22 belong to SNe Ic-bl/GRB-SNe category. We compare \( L_{\text{peak}} \) and \( t_{\text{peak}} \) of their properly constrained SNe Ic-bl/GRB-SNe with the results of our models. We show the comparison in Fig. 10. The shaded regions show the parameter space spanned by our models 2–9 for polar and equatorial viewing angles. We see that our results span a subset of the parameter space occupied by the reconstructed SNe, with the range of rise times nearly consistent with the reconstructed SNe and the range of peak bolometric luminosities falling short of the brightest reconstructed SNe. However, all values fall well within the limits of observed SNe Ic-bl. Interestingly, we find that our models with opening angles extracted from \( \beta = 0.3 \) (and not 0.1) show better agreement with the observed SNe Ic-bl indicating that wider outflows may fit SNe observations more easily.

We show the spectra at various times for our most realistic model (model 2) along with the associated uncertainties for polar and equatorial viewing angles in Fig. 11. The equatorial spectra have been shifted vertically with respect to the polar spectra for clarity. We show the spectra for individual models in Fig. 12. The viewing angle dependence is more pronounced at earlier times before the bolometric peak, while the late-time spectra show little viewing angle dependence. The uncertainties are higher for both polar and equatorial viewing angles before the bolometric peak. We find that the spectra after peak show little uncertainty and thus are robust across all models. There is some model variation for late-time polar spectra in the wavelength range 4000–5000 Å, but these are due to the variation of amounts of explosively synthesized \(^{56}\)Ni/Co/Fe along the pole for different models, which has strong bound–bound transitions in this wavelength range and increases the line opacity differently in different models. The variation in \(^{56}\)Ni distribution for different models can be seen in Fig. 8.

B2018 compared their model spectra with observed SNe Ic-bl and found that their model spectra reproduce the major characteristics of SNe Ic-bl spectra. We find that our model spectra are similar to the model spectra of B2018, with the presence of characteristic broad lines typical of a SN Ic-bl. Also, our spectra for \( t > t_{\text{peak}} \) are nearly consistent across various models and viewing angles. We conclude that within this end-to-end simulation set-up, the jetted outflow from a rapidly rotating 3D CCSN simulation is compatible with SNe Ic-bl light curves and spectra.

A SN Ic-bl can be launched even if the jet engine fails to produce a GRB. We use the scaled terminal Lorentz factor \( \gamma h \), where \( \gamma \) is the Lorentz factor and \( h \) is the specific enthalpy of the fluid scaled by \( c^{-2} \), to determine whether a particular engine model produces a GRB. We track the evolution of \( \gamma h \) and assume that material with \( \gamma h \gtrsim 10 \) post breakout constitutes a GRB if the total energy in the material with \( \gamma h \gtrsim 10 \) is greater than \( \sim 10^{50} \) erg. We find that models 1, 2, 4, 6, and 8, which have \( h_{\text{eng}} \sim 11 \), produce a successful GRB. We do not observe a GRB in models 3, 5, 7, and 9, which have \( h_{\text{eng}} \sim 17 \). This implies that narrower jet outflows provide more suitable conditions for the formation of GRBs. SN Ic-bl’s without GRBs may be associated with wider outflows. Analyzing the GRB properties in more detail will be carried out in future work.

4 CONCLUSIONS AND DISCUSSION

B2018 carried out end-to-end SRHD and radiation transfer simulations with a single central engine and successfully produced light curves and spectra nearly consistent with observations of SNe Ic-bl for a presumed set of engine parameters. In this work, we have extended their numerical set-up and instead of presuming the values of engine parameters we extract them from the 3D CCSN simulations of Moesta et al. (2014). We find that the range of light curves obtained in our set-up have nearly consistent rise times with observations of SNe Ic-bl and their peak bolometric luminosities
Figure 12. Time evolution of the spectra for all models for polar and equatorial viewing angles. Model 1 is the reproduction of the spectra obtained by B2018. Model 2 is our most realistic model for the 3D CCSNe simulation parameters. The differences from models 3–9 are the source of the shaded region in Fig. 11.
Our most realistic $E_{\text{eng}}$ and $t_{\text{peak}}$ comes from the rate of decrease of the rotational energy for material within a 50 km radius. Our most realistic $\theta_{\text{eng}}$ comes from the material with $\beta \sim 0.1$. This provides our most realistic model (model 2) with parameters $E_{\text{eng}} = 1.725 \times 10^{52} \text{erg}, t_{\text{peak}} = 1.159 \text{s}, \text{and } \theta_{\text{eng}} = 10.63^\circ$. Interestingly, this is very close to the engine parameters presumed by B2018 ($E_{\text{eng}} = 1.8 \times 10^{52} \text{erg}, t_{\text{peak}} = 1.1 \text{s}, \text{and } \theta_{\text{eng}} = 11.5^\circ$). However, in the analysis of our other models, we find that our models which use $\theta_{\text{eng}}$ extracted from the material with $\beta \approx 0.3$ (extracted $\theta_{\text{eng}} \approx 17^\circ$) show better agreement with observed $t_{\text{peak}}$ and $\theta_{\text{peak}}$ of SN Ic-bl light curves compared to the models using $\beta \sim 0.1$ (extracted $\theta_{\text{eng}} \approx 11^\circ$). This is likely due to the jet coupling more easily to the stellar material for larger opening angles which also leads to a higher $^{56}\text{Ni}$ mass synthesized during the explosion.

The JET simulations performed in this work are 2D. In future work, we plan to use 3D JET and SEDONA simulations and include magnetic fields. We have not included magnetic fields in this work because MHD simulations in 2D versus 3D show fundamentally different results (Moesta et al. 2014; Bromberg & Tchekhovskoy 2016). We will also explore more accurate methods for extracting central engine parameters from the CCSN simulation data in future work. There is also a need for longer 3D CCSN simulation data to better extract the late-time behaviour of the engine. In this way, we can reduce the uncertainty arising from the extrapolation over a time-scale of 1 s. This is challenging due to high computational cost of 3D CCSN simulations (~a month on ~1000 nodes) but will be enabled by the advent of GPU-based codes that will reduce the computational time considerably and lead to availability of data over longer time-scales. This work uses the central engine parameters extracted from a single CCSN simulation, which may not be representative of the full extent of possible parameters. Performing the present analysis for other CCSN simulations will help check the consistency of the current results as well as explore the full range of possible parameters, and then the full range of possible light curves and spectra.

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The data underlying this article will be shared on reasonable request to the corresponding author.

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