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Dynamically inflated wind models of classical Wolf-Rayet stars

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ABSTRACT

Context. Vigorous mass loss in the classical Wolf-Rayet (WR) phase is important for the late evolution and final fate of massive stars.

Aims. We develop spherically symmetric time-dependent and steady-state hydrodynamical models of the radiation-driven wind outflows and associated mass loss from classical WR stars.

Methods. The simulations are based on combining the opacities typically used in static stellar structure and evolution models with a simple parametrised form for the enhanced line opacity expected within a supersonic outflow.

Results. Our simulations reveal high mass-loss rates initiated in deep and hot, optically thick layers around $T \approx 200$ kK. The resulting velocity structure is non-monotonic and can be separated into three phases: (i) an initial acceleration to supersonic speeds (caused by the static opacity), (ii) stagnation and even deceleration, and (iii) an outer region of rapid re-acceleration (by line opacity). The characteristic structures seen in converged steady-state simulations agree well with the outflow properties of our time-dependent models.

Conclusions. By directly comparing our dynamic simulations to corresponding hydrostatic models, we explicitly demonstrate that the need to invoke extra energy transport in convectively inefficient regions of stellar structure and evolution models, in order to prevent drastic inflation of static WR envelopes, is merely an artefact of enforcing a hydrostatic outer boundary. Moreover, the dynamically inflated inner regions of our simulations provide a natural explanation for the often-found mismatch between predicted hydrostatic WR radii and those inferred from spectroscopy; by extrapolating a monotonic $\beta$-type velocity law from the observable supersonic regions to the invisible hydrostatic core, spectroscopic models likely overestimate the core radius by a factor of a few. Finally, we contrast our simulations with alternative recent WR wind models based on co-moving frame (CMF) radiative transfer to compute the radiation force. Since CMF transfer currently cannot handle non-monotonic velocity fields, the characteristic deceleration regions found here are avoided in such simulations by invoking an ad hoc very high degree of clumping.

Key words. stars: mass-loss – stars: Wolf-Rayet – stars: winds, outflows – stars: atmospheres

1. Introduction

The evolution of the Sun with initial masses higher than eight times that of the Sun plays an essential role in the chemistry and dynamics of galaxies similar to our Milky Way (Crowther 2007; Doran et al. 2013; Ramachandran et al. 2018; Prantzos et al. 2018). These massive stars are a vital source of heavy elements and UV radiation, enriching their surroundings through strong radiation-driven winds (Lucy & Solomon 1970; Castor et al. 1975; Puls et al. 2008; Vink et al. 2001; Bjorklund et al. 2021). In the final evolutionary stages, some of those massive stars become hydrogen-depleted, usually core He-burning progenitors of neutron stars or black holes (Yoon et al. 2012; Groh et al. 2013). Among these are so called classical Wolf-Rayet (WR) stars (Wolf & Rayet 1867), which are characterised by strong spectral emission lines and a high luminosity to mass ratio, $L/M_\odot \sim 10^4 L_\odot/ M_\odot$ (Crowther 2007). Classical WR stars are distinct from very massive, main-sequence WR stars, which are core H-burning (de Koter et al. 1997; Crowther et al. 2010). Classical WR stars are also different in their composition and evolutionary state from hydrogen-deficient WR central stars of planetary nebula (e.g. Todt et al. 2010).

As first suggested by Beals (1929), the prominent emission lines visible in WR spectra indicate strong stellar winds with high terminal speeds ($v_{\infty} \sim 2000-3000$ km s$^{-1}$) and mass-loss rates ($\dot{M} \sim 10^{-5}-10^{-3}$ $M_\odot$ yr$^{-1}$) (Hamann et al. 2019; Sander et al. 2019). However, while the overall wind properties of massive main-sequence OB-stars (see Puls et al. 2008 for a review) are rather well reproduced by the line-driven wind theory formulated first by Castor et al. (1975; CAK), this standard theory typically fails to explain the order of magnitude higher mass-loss rates of classical WR stars (Cassinelli 1991; Lamers & Leitherer 1993).

Nonetheless, WR winds are still thought to be radiation driven, as their high $L/M_\odot$ ratio brings them close to the limit at which the acceleration due to radiation $g_r$ balances that of gravity $g$ (i.e. close to $\Gamma = 1$, for Eddington factor $\Gamma = g_r/g$). In fact, consulting the opacities used in stellar structure calculations, which are generally obtained from tabulations computed assuming a static medium (e.g. Iglesias & Rogers 1996), the Eddington limit for classical WR stars is already reached in sub-surface layers with temperatures of about 150–250 kK. Since convection is highly inefficient in these layers (Gräfenet al. 2012), static models then typically display density inversions and highly inflated stellar envelopes (Ishii et al. 1999; Petrovic et al. 2000; Gräfenet al. 2012; Sanyal et al. 2015). For corresponding stellar evolution calculations, such envelope inflation is computationally difficult to treat and various numerical tricks are thus typically required to make computations tractable (Paxton et al. 2013; Ekström et al. 2012). This then leads to very hot
(\(T_{\text{eff}} \gtrsim 100\,\text{kK}\)) and compact (\(R \sim R_\odot\)) WR stellar surfaces. On the other hand, spectroscopic studies aiming to constrain the WR surface from observationally inferred \(T_{\text{eff}}\) typically deduce hydrostatic radii that are factors of \(~2\)–\(~3\) higher than predicted by such evolution models (e.g. Crowther 2007; Sander et al. 2019; Hamann et al. 2019); this mismatch is sometimes referred to as the core-radius problem of classical WR stars.

Rather than retaining a static envelope, breaching the Eddington limit in sub-photospheric layers can initiate an optically thick supersonic outflow. Nugis & Lamers (2002) and Grassitelli et al. (2018) suggested that WR mass-loss rates can be computed simply by considering only the conditions at the point where the sonic speed is reached (at \(\Gamma \approx 1\), since gas pressure terms are very small in comparison). Using the OPAL tables of Rosseland mean opacity (Iglesias & Rogers 1996), Ro & Matzner (2016) showed that supersonic velocities are indeed found in deep sub-photospheric layers, but that a successful wind solution that could bring the initiated mass flux to infinity could not be found.

However, these models neglect the strong enhancement of the line opacity expected in a supersonic outflow. Previous modelling attempts including the Doppler effect in the line opacity calculations have either relied on a pre-assumed fixed velocity field to solve for the mass loss (e.g. see Lucy & Abbott 1993; Springmann 1994; Springmann & Puls 1998; de Koter et al. 1997), or attempted an iterative (assuming time independence) solution towards a self-consistent velocity field and mass loss (Gräfener & Hamann 2005; Sander et al. 2020; Sander & Vink 2020). The latter models have used comoving-frame (CMF) radiative transfer for the calculation of \(g_\nu\). Such CMF transfer is a computationally intensive numerical technique that requires the velocity field to remain smooth and monotonic (see, e.g. discussion in Sander et al. 2020). Moreover, all these previous studies of classical WR outflows have been performed in the steady-state limit.

In this paper we present a first attempt to build a model that addresses both (dynamic) envelope inflation and line driving, using a hybrid opacity approach based on combining the opacities used for static stellar structure calculations with a simple variant of the standard parameterisation for line opacities in supersonic flows. This formalism then allows for computation of both steady-state and time-dependent WR wind structures. The organisation of the paper is as follows: in Sect. 2, we describe our basic physical set-up. We present dynamical models in the steady-state limit and compare these to corresponding static calculations in Sect. 3. Then in Sect. 4 we compare these steady-state models to full time-dependent radiation-hydrodynamical simulations of dynamically inflated WR outflows. In Sect. 5 we discuss our results and some open questions regarding WR stellar outflows, and finally we summarise our results and provide an outlook for future work in Sect. 6.

### 2. Physical model

We describe the WR wind outflow by the appropriate hydrodynamical equations of mass and momentum conservation assuming spherical symmetry:

\[
\frac{\partial \rho}{\partial t} + \frac{1}{r^2} \frac{\partial}{\partial r} \left( r^2 (\rho v) \right) = 0, \tag{1}
\]

\[
\frac{\partial (\rho v)}{\partial t} + \frac{1}{r^2} \frac{\partial}{\partial r} \left( r^2 (\rho v^2) \right) = - \frac{\partial P}{\partial r} - \rho g + \rho g_\nu. \tag{2}
\]

Here \(\rho\), \(v\) and \(P \equiv k_B T \rho/(\mu m_\text{H})\) are mass density, velocity and gas pressure, where \(T\) is gas temperature, \(k_B\) is the Boltzmann constant, \(\mu\) is the mean molecular weight, and \(m_\text{H}\) is the mass of the hydrogen atom. \(g \equiv g M_\star / r^2\) is the gravitation acceleration for a constant stellar mass \(M_\star\) and

\[
g_\nu = \frac{\kappa_F F}{c}. \tag{3}
\]

is the acceleration due to stellar radiation, for radiation flux \(F\) and flux-weighted opacity (mass-absorption coefficient) \(\kappa_F\) in \(\text{cm}^2\,\text{g}^{-1}\). Using the Eddington factor we can also write the equation of motion (e.o.m) as:

\[
\frac{\partial}{\partial t} (\rho v) + \frac{1}{r^2} \frac{\partial}{\partial r} \left( r^2 (\rho v^2) \right) = - \frac{\partial P}{\partial r} - \rho \frac{M_\star G}{r^2}(1 - \Gamma). \tag{4}
\]

The Eddington ratio can be expressed as:

\[
\Gamma = \frac{\kappa_F L}{4\pi M_\star G c}, \tag{5}
\]

for a stellar luminosity \(L = 4\pi r^2 F\). In this paper, we assume that the radiative luminosity remains constant throughout the outflow. This means that we neglect a term corresponding to the work of the radiation field against gravity. We can estimate the corresponding expected luminosity variation by computing the photon-tiring parameter \(m = M/M_{\text{max}}\) (Owocki et al. 2017), which is the ratio of the stellar mass loss \(M\) to the maximum amount of mass loss that the stellar luminosity can drive, \(M_{\text{max}} = L R_\odot / (L_{\odot} G)\), where \(R_\odot\) is the core radius defined at the fixed lower boundary. Taking the stellar parameters used throughout this paper, \(M_\star = 10 M_\odot\), \(R_\odot = 1 R_\odot\), \(\log(L/L_{\odot}) = 5.416\), and a typical order of magnitude mass loss, \(M \approx 5.0 \times 10^{-5} M_\odot\,\text{yr}^{-1}\), one gets

\[
m = \frac{M G M_\star}{R_\odot L} \approx 0.06, \tag{6}
\]

which demonstrates that the luminosity variation is only a marginal effect for the cases considered in this paper.

In practice, especially for time-dependent dynamical computations with possibly non-monotonic velocity fields, it is not computationally feasible to derive the temperature structure, for example, from radiative equilibrium by means of full solutions to the frequency-dependent radiative transfer equations. To simplify, we therefore follow the common approach of replacing the full energy equation by the Lucy (1997) analytic radiative equilibrium model for a grey, spherically symmetric, diluted atmosphere, however, replacing the grey opacity by the actual flux weighted \(\kappa_F\) (e.g. see Lucy & Abbott 1993). This allows us to write the temperature structure as:

\[
T^4 = T_{\text{c,eff}}^4 \left( \frac{W(r)}{3} + \frac{3}{4} \tau_{\text{sp}} \right), \tag{7}
\]

where \(T_{\text{c,eff}}^4 = L/(4\pi \sigma_{SB} R_\odot^2)\) is a core effective temperature, defined here from the lower boundary set at \(R_{\text{c,SB}}\) is the Stefan-Boltzmann constant, \(W(r) = 0.5 \left(1 - \sqrt{1 - R_{\odot}^2/r^2}\right)\) is the dilution factor, and \(\tau_{\text{sp}}\) is the spherically modified optical depth

\[
\tau_{\text{sp}} = -\kappa_F \rho \left( \frac{R_\odot}{r} \right)^2 dr, \quad \text{or} \quad \tau_{\text{sp}} = \int_r^\infty dr' \kappa_F \rho \left( \frac{R_\odot}{r'} \right)^2. \tag{8}
\]
Here again the radius of our fixed lower boundary \(R_c\) is used as a scaling radius for the spherically modified optical depth scale. This is similar to the WR models by Sander et al. (2020) who also define their stellar radius from the hydrostatic lower boundary. It is different, however, than, for example, Sundqvist et al. (2019) who set the reference radius for the temperature structure in their O-star models at a photospheric radius \(R_{\text{ph}}\). An argument against using \(R_{\text{ph}}\) as a scaling radius for optically thick WR winds is, however, that \(R_{\text{ph}} \gg R_c\) such that the geometric dilution of the radiation field would be neglected for large parts of the outflow (see also discussion in Nugis & Lamers 2002). In principle, the explicit choice of the reference radius will affect the temperature structure throughout our models. However, test calculations have shown that this is a quite marginal effect for the resulting mass loss and velocities of the simulations considered in this paper. In any case, to facilitate comparison with other models we also introduce a stellar photospheric effective temperature \(T_{\text{ph, eff}}\) at this photospheric radius \(R_{\text{ph}}\). Since the definition of a stellar photosphere in a spherically diluted stellar envelope is non-trivial\(^1\) and depends on the specific computation of the temperature structure, we here simply approximate

\[
T(R_{\text{ph}}) = \frac{L}{4\pi R_{\text{ph}}^2 \tau_{\text{ph}}} \equiv T_{\text{ph, eff}},
\]

such that the photospheric and core effective temperatures and radii are related through

\[
T_{\text{ph, eff}} = \sqrt{\frac{R_c}{R_{\text{ph}}} T_{\text{c, eff}}}. \tag{10}
\]

For given stellar parameters \(L, M_*,\) and \(R_c\), and a known variation of \(\kappa_f\), Eqs. (1)–(8) form the basic system of coupled differential equations under investigation in this paper. In general, \(\kappa_f\) is a complicated function that depends on chemical composition, density, temperature, velocity and radial position of the absorbing and emitting gas. In this study, we focus on two cases. First, we consider static opacities such as those used for stellar structure and evolution computations (see Ro & Matzner 2016). Due to the high continuum optical depth of WR outflows, conditions in the wind launching regions resemble those of radiative diffusion, allowing us to replace the flux-weighted opacity with a Rosseland mean, and so to utilise standard OPAL tables for the opacity mapping as a function of \(T\) and \(\rho\) (Iglesias & Rogers 1996). However, since these tabulations ignore the influence of Doppler shifts on the line opacity (which are critical for WR wind driving, e.g. Sander et al. 2020), we also consider a hybrid model accounting at least approximately for this effect. More specifically, we use a CAK-like parametrisation to add the cumulative force from an ensemble of spectral lines to the OPAL tables (see, Sect. 3.3).

\section{3. Steady-state approximation}

To build physical insight we first examine a simplified steady-state case. Equations (1) and (4) are then written as:

\[
M = 4\pi r^2 \rho v = \text{constant}, \tag{11}
\]

\[
\left(1 - \frac{\alpha_r^2}{r^2} \right) \frac{dv}{dr} = \frac{2\alpha_r^2}{r} - \frac{d\alpha_r^2}{dr} - \frac{M_* G}{r^2} (1 - \Gamma), \tag{12}
\]

\(^1\) For example, in Sect. 3.6 the stellar photoshere is located at the \(\tau_{\text{ph}} = 4/3\) surface in the radiation diffusion approximation, rather than the typically assumed photosphere location at the \(\tau_{\text{ph}} = 2/3\) surface.

for an isothermal sound speed \(\alpha_r^2 = k_B T/(\mu m_H)\). Equation (11) defines the spherically symmetric mass-loss rate \(M\). Here we assume \(\mu = 4/3\) corresponding to a fully ionised helium plasma.

It is commonly believed that the winds of WR stars are initiated in the deep sub-photospheric layers where the gas temperature is \(T \sim 150–200\, KK\). In this temperature region, due to iron recombination, a significant increase of the Rosseland mean opacity is observed, sometimes called the iron opacity bump. A simple comparison of scales reveals that throughout the supersonic wind outflow the first two terms of the r.h.s. in Eq. (12) are much smaller than the radiation and gravitation terms, so that we can approximate the e.o.m with

\[
\frac{1}{2} \left(1 - \frac{\alpha_r^2}{r^2}\right) \frac{d\alpha_r^2}{dr} = \frac{M_* G}{r^2} (1 - \Gamma). \tag{13}
\]

Here, the sound-speed term on the l.h.s. is retained in order to enable a mapping of the supersonic solution onto the subsonic part.

\subsection{3.1. Boundary conditions}

Equations (7)–(13) impose a two-point boundary value problem, with boundaries at \(R_c\) and \(r \to \infty\). The inner boundary at \(r = R_c\) is defined to be a sonic point, with \(v^2 = a^2 e^2\), where \(a_e\) is defined to be the sound speed at this sonic point. As can be seen from Eq. (13), this implies \(\Gamma(R_c) = 1\). Below the sonic point as the velocity rapidly diminishes from its sonic point value \(a_e\) inwards, the density structure is well approximated by the hydrostatic solution (e.g. see Ro & Matzner 2016; Grassitelli et al. 2018). In contrast, in the supersonic part, the density structure diverges from the structure given by the hydrostatic solution. As such, we initiate the calculation at the sonic point and only consider the supersonic part of the outflow, assuming that the sub-sonic region still can be described by hydrostatic equilibrium. The tabulated OPAL opacities can then be used to locate points for which \(\Gamma = 1\), constraining the lower boundary density as a function of temperature. In this way, the range of possible mass-loss rates \(M = 4\pi R_{\text{ph}}^2 a_e a_i c_i\) is set as a function of the lower boundary temperature.

The outer boundary is set by requiring that the wind temperature decreases sufficiently at large radii. Replacing density with the mass-loss rate using Eq. (11), the spherically modified optical depth (Eq. (8)) is used to compute the temperature structure according to Eq. (7). We compute the optical depth at the outer boundary \(\tau_{\text{out}}\) by radially integrating Eq. (8) in \(r \in [R_{\text{max}}, \infty)\), assuming a terminal velocity \(v(r \geq R_{\text{max}}) = v(R_{\text{max}}) = \bar{v}_c\) and \(\kappa_f(r \geq R_{\text{max}}) = \kappa_c\), where \(\kappa_c\) is the Thompson scattering mass absorption coefficient. The outer boundary temperature is then set by the maximum between applying \(\tau_{\text{out}}\) in Eq. (8) and a floor value, which is typically set to a few tenths of the stellar effective temperature (see Puls et al. 2005; Sundqvist et al. 2019). By matching the inner and outer boundary constraints, we uniquely constrain the wind structure. In turn this then sets the unique mass-loss rate of the model from the range of possible solutions at the lower boundary.

\subsection{3.2. Energy requirement}

Additionally, for wind material to escape the stellar potential, the global energy requirement must be satisfied, which means that the integrated mechanical energy of the wind has to be positive.

\footnote{For numerical computations the outer formal boundary is simply replaced by a maximum radius \(R_{\text{max}} \gg R_c\).}
Taking the supersonic limit $a^2/v^2 \ll 1$ in Eq. (13) yields:

$$\frac{v^2_{\text{esc}}}{2} - \frac{v^2_0}{2} = \frac{v^2_{\text{esc}}}{2} \int_{R_e}^{\infty} \frac{R \Gamma}{r^2} dr - \frac{v^2_{\text{esc}}}{2}. \quad (14)$$

Here $v_0 \sim a_s$ is the initial velocity and $v^2_{\text{esc}} = 2M_* G / R_e$ is the escape velocity from $R_e$. The first term on the r.h.s. corresponds to the work done by the stellar radiation and the second term is the work done by gravity. We can then introduce $\mathcal{W}$ as the net energy change in units of $v^2_{\text{esc}}/2$:

$$\mathcal{W} = \int_{R_e}^{\infty} \frac{R \Gamma}{r^2} dr - 1. \quad (15)$$

For the wind to escape to $r \to \infty$, this net energy change has to be positive, that is $\mathcal{W} \geq 0$. Alternatively, we can also introduce the ratio of kinetic to core potential energy as a square of the velocity to core escape velocity ratio:

$$w(r) = \left(\frac{v(r)}{v_{\text{esc}}}\right)^2, \quad (16)$$

which goes to $\mathcal{W}$ as $r \to \infty$ so that by construction we require $w(r \to \infty) > 0$ in order to escape.

### 3.3. Failed Winds in the static opacity limit

We first investigate the possibility of driving the stellar outflow in the static opacity limit, i.e. the limit in which we only consider OPAL opacities, thus neglecting the Doppler effect; $\kappa_F = \kappa_{\text{OPAL}}$ (see also Ro & Matzner 2016). To set up the problem, we choose the stellar mass and the core radius (as given in Table 1) such that they roughly represent the average value of the mass-to-radius ratio of the observationally inferred WR stellar population from Hamann et al. (2019) and Sander et al. (2019). The luminosity is then set such that the resulting $\Gamma_e = 0.40$, also corresponding to the observationally inferred average (Hamann et al. 2019; Sander et al. 2019).

The natural candidate for the missing opacity source discussed above comes from the cumulative effect of spectral lines due to OPAL opacities thus neglecting the Doppler effect.

### Table 1. Summary of stellar parameters used in this paper.

<table>
<thead>
<tr>
<th>$M_*/M_\odot$</th>
<th>$R_*/R_\odot$</th>
<th>$\log(L/L_\odot)$</th>
<th>$v_{\text{esc}}$ (km s$^{-1}$)</th>
</tr>
</thead>
<tbody>
<tr>
<td>10</td>
<td>1</td>
<td>5.416</td>
<td>1950</td>
</tr>
</tbody>
</table>

**Notes.** Here we set our standard stellar parameters such that they roughly represent the average value of the mass-to-radius ratio of the observationally inferred WR stellar population from Hamann et al. (2019) and Sander et al. (2019). The luminosity is then set such that the resulting $\Gamma_e = 0.40$, also corresponding to the observationally inferred average (Hamann et al. 2019; Sander et al. 2019).

### Fig. 1. (a) Colour map of $\Gamma_{\text{OPAL}}$ for the stellar parameters from Table 1. Temperature is given on the abscissa and radiation-to-gas pressure ratio on the ordinate. $\Gamma(\rho_s, a^2) = 1$ is identified with a white contour. The colour bar on the right corresponds to the colour coding of the plot and gives the numerical value of $\Gamma_{\text{OPAL}}$ for a given temperature and radiation-to-gas pressure ratio. Different line styles show the radiation-to-gas pressure ratio and temperature structure for the different fixed mass-loss rates. (b) Ratio of kinetic to core potential energy $w = v^2 / v^2_{\text{esc}}$ of the corresponding solutions from panel a. The abscissa here shows the radius coordinate $x$.

and gas pressure $P_g$ on the ordinate (the ratio $P_t/P_g$ is a proxy for the density). The integration curves show the density and temperature structure for the different cases, starting from various positions on the $\Gamma = 1$ curve at the inner boundary $R_e$ and extending outwards. Figure 1b then shows the corresponding net gain of kinetic energy (Eq. (16)), demonstrating that after an initial acceleration and increasing velocities, all of the curves start to decelerate until eventually reaching zero velocity and so terminating the outward integration (some solutions had to be formally terminated before actually reaching zero velocity, due to numerical difficulties in the steep deceleration region). This indicates that none of the potential solutions starting from the $\Gamma = 1$ curve are able to escape the stellar gravitational potential. These results are consistent with Ro & Matzner (2016), who also found that OPAL opacities were not able to sustain a radiation-driven mass loss initiated in the deep layers around the iron bump, and indicates that an additional source of opacity is required, raising the question of a missing force.

### 3.4. Missing force

The natural candidate for the missing opacity source discussed above comes from the cumulative effect of spectral lines due to...
the Doppler effect. To estimate this we use the CAK parametrisation for a distribution of spectral lines, using here a simple approximation of taking the absolute value of the velocity gradient:

\[
\Gamma_{\text{CAK}} = \Gamma_r \left( \frac{1 - \alpha}{\kappa_{\text{CAK}}} \right)^2 |\frac{dv}{dr}|^\alpha,
\]

where \( \Gamma \) is an effective strength of the line ensemble (Gayley 1995), and \( \alpha \) sets the CAK line distribution power index. In reality, once regions where \( dv/dr < 0 \) arise, it is possible for a photon proceeding from the stellar core to be Doppler shifted into resonance with the same spectral line at multiple locations in the outflow, thereby requiring a fully non-local computation of the line acceleration. As discussed further below, this could (in principle) be handled in a more self-consistent manner by, for example, Monte-Carlo (MC) line-force calculations. In this initial study, however, we opt for a simpler approach, in order to make time-dependent simulations feasible as well. Two possible approximations that can be taken then are to either take the absolute value of the velocity gradient \( |dv/dr| \) or use \( \max(0,v/dr) \). The first approach estimates (approximately) an upper limit to the CAK-like force in regions with negative velocity gradients, whereas the second approach would correspond to a lower limit. As most previous studies of line-driven dynamical flows have used \( |dv/dr| \) (for example, in investigations of line-driven winds from rapidly rotating stars, Petrenz & Puls 2000, and around discs, Proga et al. 1998; Kee et al. 2016), we follow this standard approach in this paper. However, test computations using instead the lower limit \( \max(0,v/dr) \) show that although some details of the radiation force profile then change, none of our conclusions are affected. With this approximation, using Eq. (18) for \( \Gamma_{\text{CAK}} \) then accounts for the force from spectral lines in super-sonic regions, while \( \Gamma_{\text{OPAL}} \) handles the force from the continuum and spectral lines in the static limit. As such, the total radiative acceleration can be simply estimated by the sum of the CAK-like contribution and the static OPAL opacities, \( \Gamma_{\text{tot}} = \Gamma_{\text{OPAL}} + \Gamma_{\text{CAK}} \).

Let us note here directly that the CAK line force is originally derived for application in winds that are optically thin for continuum radiation. In the lower layers of the dense WR outflows considered here, this will typically not be the case. A more rigorous treatment would then also need to take into account the change in continuum intensity by solving the transfer equation for line+continuum opacities. While approximations for the diffusion limit exist (Gayley et al. 1995) no general formalism has been developed. As such, in this first study of WR wind dynamics we opt for the simple radial-streaming CAK form above.

Furthermore, due to the explicit dependency of the CAK line force on \( dv/dr \) the sonic point is now formally not a critical point (see Castor et al. 1975). However, our iteration scheme circumvents this issue by always applying the velocity gradient from the sonic regions, while \( \Gamma_{\text{CAK}} \) also has a significant impact on the conditions at the optically thick lower boundary at the sonic point. Assuming typical O-star values \( \alpha = 0.66, \bar{Q} = 2300 \) (e.g. Puls et al. 2000), approximating the velocity gradient\(^3\) as \( dv/dr \sim \Delta v_{\text{max}}/\Delta R(t = t_{\text{max}}) \), and using the mass density and velocity computed in the static opacity limit for \( M = 5.0 \times 10^{-5} M_\odot \text{ yr}^{-1} \), we find the Eddington ratio for the CAK force at the lower boundary to be \( \Gamma_{\text{CAK}} = q_{\text{CAK}}/q \sim 0.1 \). Such a small contribution from the CAK force is not surprising due to the high density at the lower boundary\(^4\) \( (\Gamma_{\text{CAK}} \sim 1/\rho^2, \text{ with } \alpha > 0) \). However, from test calculations it turns out that although the CAK contribution indeed increases as we move outwards in the wind, a simple model with constant \( \alpha = 0.66, \bar{Q} = 2300 \) is still not able to provide the force necessary to achieve a positive total wind energy and so drive the wind to infinity (see previous section).

There are, however, several indications that the line force in the outer winds of classical WR stars indeed might be significantly enhanced as compared to O-type stars. For example, the independent MC line-force calculations by Lucy & Abbott (1993) and Springmann & Puls (1998) both find global momentum rates for WR stars that exceed those of O-stars by an order of magnitude or more. In these MC computations, the outer-wind enhancement of the line force stems from the decreasing level of ionisation with increasing distance from the star in the optically thick WR outflows. Due to this shift from high-to-low ionisation stages as photons move outwards in the wind, new spectral lines become available for photons to interact with. As these new lines have different interaction frequencies than those previously available in the inner wind parts, this means that the line-frequency gaps typically observed for the nearly constant (frozen-in) ionisation conditions of optically thin O-star winds are effectively closed. This then leads to photon trapping (Lucy & Abbott 1993) and efficient multi-line scattering, which significantly increases the line force.

To mimic the effect of an outer wind line-force enhancement, we introduce here a simple spatial variation \( \alpha = \alpha(r) \), which increases the CAK force away from the star by a modest decrease of \( \alpha \). To this end, we assume \( \alpha(r) \) as a piecewise linear function with a constant \( \alpha_{\text{max}} \) from the lower boundary to \( r_1 \) and a constant \( \alpha_{\text{min}} \) from \( r_2 \) to the outer boundary, interpolating between the two values in the range \( [r_1, r_2] \). This then allows the wind outflow initiated at the lower boundary to achieve positive total energy, and so be sustained until the upper boundary. While the specific treatment of \( \alpha \) is done here in an ad hoc manner, the overall assumed form is quite consistent with the multi-scattering line-force enhancement found in the MC line-force computations for a CAK-like spectral line distribution by Springmann (1994). The approximate values of \( \alpha(x) \) that correspond to the line force computed by Springmann (1994) are given in Fig. 2 as black asterisks, with the \( \alpha(x) \) as adapted in the standard model of this paper over-plotted as a solid line. The figure shows that the order of magnitude outer-wind line-force enhancement applied here indeed is on the same order as that found in these MC calculations.

We note, however, that the Springmann (1994) calculations were performed only for parameterised (monotonic) \( \beta \)-type velocity laws. As such, there is not a complete one-to-one correspondence between the spatial and velocity scales in these MC

\(^3\) We define \( t_{\text{max}} \) as the maximum velocity found for the given fixed mass loss in the static opacity limit.

\(^4\) The numerical simulations presented in Sects. 3–4 a posteriori confirm the simple order of magnitude estimate made here, showing explicitly that the force contribution from the CAK-like opacities near the lower boundary indeed is very small for our considered cases (see, e.g. Fig. 3c). This thus resolves some potential issues of our basic approach (simple summation of OPAL and CAK-like opacities) regarding double counting the effect of spectral lines in the static limit.
the optical depth found in the first step. The mass-loss rate is
computed following (ii) an outside-in integration where velocity,
 density, and temperature structure are computed, fol-
lowing (i) an inside-out integration to describe the cor-
responding variation of $\alpha$. The vertical dashed lines corre-
spond to $r_1$ ($x_1$) and $r_2$ ($x_2$).

calculations and those of the present paper. Nonetheless, the
overall similarity with the very simple radial dependence of the
$\alpha$ parameter adopted here is encouraging. In a follow-up work,
we plan to couple the hydrodynamic simulations presented here
directly to such MC computations, building on the method devel-
oped by Puls et al. (2000) for proper estimation of occupation
numbers, and accounting fully for multi-scattering effects as well
as non-monotonic velocity fields.

As outlined in detail in the following sections (for our stan-
dard values listed in Table 2) the formalism outlined above gives
rise to dynamically inflated wind solutions, where the structure
in the optically thick deep layers near the iron bump is primarily
governed by $\Gamma_{\text{OPAL}}$ but where $\Gamma_{\text{CAK}}$ takes over the driving in the
dilated outer regions. This then causes a typical wind structure
that is characterised by a high mass-loss rate from the
lower boundary, a slow (end even partially negative) acceleration
of the deeper layers, and a rapid re-acceleration of the outer
wind. As such, the typical velocity laws we find not only dra-
scially deviate from the standard $\beta$-type laws assumed by most
atmospheric models, but they also contain a significant region of
negative acceleration (see also Fig. 14 in Pauldrach et al. 1993).

### 3.5. Dynamically inflated steady-state model

Based on the hybrid formalism introduced above we can now
numerically solve Eqs. (7)–(13), iterating convergence using a simple scheme based on Runge-Kutta integrations. As
discussed in Sect. 3.1, to constrain the mass-loss rate it is critical
to here take into account the two-point boundary value nature of
the problem. At a basic level, every iteration is performed using two
steps: (i) an inside-out integration $R_e \rightarrow R_{\text{max}}$, where the
velocity, density, and temperature structure are computed, fol-
lowing (ii) an outside-in integration $R_{\text{max}} \rightarrow R_e$ updating the
temperature structure using the correct boundary condition from
the optical depth found in the first step. The mass-loss rate is
then updated for the next iteration by finding the correct loca-
tion on the $\Gamma = 1$ curve at the lower boundary, using the updated
temperature structure from the outside-in integration.

Using this scheme, Fig. 3a shows the final, converged tem-
perature profile for our standard stellar parameters (Table 1) and
choice of line-force parameters (Table 2). The final (also con-
verged) mass-loss rate for the model is $\dot{M} = 1.47 \times 10^{-5} \, M_\odot \, \text{yr}^{-1}$.

In addition to a high predicted mass-loss rate, the solution
displays a non-monotonic velocity field. The resulting velocity
profile shown in Fig. 3b can be split into three basic regions: (1)
an initial acceleration from the core followed by (2) stagnation and even a deceleration part (and so a negative velocity gradient, marked with crosses in the figure), and (3) an outer region of fast re-acceleration to outflow velocities $>1000 \, \text{km s}^{-1}$. The distinc-
tive behaviour of these three regions can be understood via the
different contributing parts of the total radiation force.

Figure 3c illustrates this, plotting the individual contribu-
tions of OPAL and CAK-like opacities to the total radiative acceleration. From the figure, on one hand, it is clear that in the
inner regions the radiation force is dominated by OPAL opacities
and the CAK-like contribution is small; indeed, the sonic point
conditions at the lower boundary can here be quite well approx-
imated using only OPAL opacities, i.e. neglecting any influence
from the Doppler-shift enhancement of line opacities. On the
other hand, in the outer regions $\Gamma_{\text{CAK}}$ becomes the dominant
part, causing a re-acceleration of the flow and setting a high ter-
mal wind velocity. This re-acceleration ensures that the energy
requirement of Eq. (15) is satisfied. As such, it is this part that
ultimately allows the wind to be sustained all the way to the outer
boundary, in contrast to the failed outflow and fallback seen in
the previous section.

To explore the influence of different opacity contributions
on the mass loss of the model, we explore the logarithm of the
spherically modified optical depth (Eq. (8)) as a function of
radius in Fig. 3d. The dashed vertical line marks the location of
the stellar photosphere defined by Eq. (9). We note, however, that,
at the photosphere $r_{\text{ph}}(R_{\text{ph}}) \neq 2/3$ as $R_e$ is used as a scaling radius in
Eq. (8). For most stars, this photospheric radius $R_{\text{ph}}$ serves
as the hydrostatic stellar radius; by contrast, for the WR stars
examined in this paper, the photosphere is located well in the
outflowing regions. Inspection of Fig. 3d shows that the majority
of $\tau_{\text{ph}}$ is accumulated within few stellar radii in the regions dom-
inated by OPAL opacities, thus the converged lower boundary
temperature, and thus the mass-loss rate, is primarily controlled
by $\Gamma_{\text{OPAL}}$.

Inspection of the density distribution in Fig. 3e further clar-
ifies the terminology dynamic inflation. In this figure, we have
gained a good identification of the location $R_{\text{sh}}$ with a vertical dashed line.
The figure shows a relatively slow decline of the density in the
sub-photospheric parts, which is somewhat reminiscent of the
profiles seen in hydrostatic stellar models near the Eddington
limit that undergo envelope inflation (see further below). But
unlike such static inflation models, the simulations here allow
for a velocity field to develop; the low-density envelope now
represents a dynamically inflated star.

### 3.6. Comparison to static inflation

For the same lower boundary conditions as adopted above, we
can also compute static models. This can then serve as a direct
comparison between the dynamic inflation found in the models
above, and the static inflation that often occurs in stellar struc-
ture models neglecting the $v_{\text{infl}}/dr$ term in the e.o.m. (and so
assuming a hydrostatic stellar envelope throughout, e.g. Petrovic et al. 2006; Gräfener et al. 2012).

To construct such static models, we simply set \( v \sim \frac{dv}{dr} \approx 0 \) in our steady-state e.o.m. above. Introducing a column mass \( \frac{dr}{dm} = \frac{1}{\rho} \), we write the resulting equation of hydrostatic equilibrium as:

\[
\frac{dP_g}{dm} = -\frac{M_gG}{r^2} (\Gamma - 1).
\]

(20)

We further simplify the temperature calculation by assuming radiative diffusion in these optically thick hydrostatic layers:

\[
\frac{dP_r}{dm} = -\frac{M_rG}{r^2} \Gamma,
\]

(21)

for a radiation pressure according to Eq. (17). Combining the equations for gas and radiation pressure, one obtains

\[
\frac{dP_g}{dP_r} = \frac{1 - \Gamma}{\Gamma}.
\]

(22)

where now \( \Gamma = \Gamma_{\text{OPAL}} \) throughout the complete model.

This set-up imposes a similar two-point boundary value problem as previously analysed. To provide a fair comparison with those dynamical simulations, we assume the same lower boundary radius \( r = R_c \) as before and re-use the lower boundary temperature \( T \approx 230 \text{kK} \) found from the converged hydrodynamic steady-state model presented above. However, at this inner boundary we now impose \( \Gamma < 1 \) as \( \Gamma \geq 1 \) would lead to non-zero gas pressure at \( r \to \infty \) (see also Sect. 2.2 in Gräfener et al. 2012). The outer boundary conditions for gas and radiation pressure (i.e., density and temperature) are also set up in the same way as before. Assuming \( \Gamma = \text{const} = \Gamma_e \) for the region \( r \in [R_{\text{max}}, \infty) \), we may integrate the hydrostatic equations to estimate the temperature and the density at the outer boundary \( r = R_{\text{max}} \). This fixes the effective temperature and the spherically modified optical depth scale \( \tilde{\tau}_{\text{sp}} = -\kappa_{\text{OPAL}} \rho (R_{\text{max}}/r)^2 dr \) of these hydrostatic (HS) models, requiring that the outer boundary always satisfies \( \tilde{\tau}_{\text{sp}}(R_{\text{max}}) = 4/3 \). Thus in this model, the stellar photospheric radius is defined as

\[
\tilde{R}_{\text{ph}} \equiv r(\tilde{\tau}_{\text{sp}} = 4/3),
\]

(23)

for the corresponding hydrostatic effective temperature

\[
T_{\text{HS, eff}}^4 \equiv \frac{L}{4\pi \sigma \tilde{R}_{\text{ph}}^2},
\]

(24)

quite analogous to how these quantities typically are defined in static stellar structure and evolution models.

These boundary conditions are used to numerically solve the new set of equations from the outer boundary inwards. A consistent solution is obtained by shooting for the fixed inner boundary temperature and radius, varying the stellar photospheric radius \( \tilde{R}_{\text{ph}} \) and assuming inner-boundary values as discussed above. In this way we obtain static envelopes corresponding directly to
our previous dynamic models. The right panel of Fig. 4 shows the predicted densities for static models with different assumed $\Gamma_e \in \{0.37, 0.40, 0.41\}$ (for comparison see Fig. 1 in Gräfener et al. 2012). These densities are then compared to those of the steady-state computation in Sect. 3, for which $\Gamma_e = 0.40$.

We note directly that in the static case an extended region of low density is formed. The photospheric radius $R_{ph}$ of this inflated envelope is extremely sensitive to $\Gamma_e$, with $R_{ph}$ growing notably as $\Gamma_e$ is increased. For the static model with highest assumed $\Gamma_e = 0.41$, we already find a large $R_{ph} \approx 35R_\odot$ accompanied by a relatively cool effective temperature $T_{\text{eff, eff}} \approx 21$ K; further increasing $\Gamma_e$ causes the inferred photospheric radius to inflate to increasingly unrealistic, extremely large values. For the $\Gamma_e = 0.40$ that we use in our dynamic models we find $R_{ph} = 4.7R_\odot$ and $T_{\text{eff, eff}} \approx 56$ K. The reason for the inflation here is the same as in the models by Petrovic et al. (2006) and Gräfener et al. (2012). Basically, it is related to the fact that for high values of $\Gamma_e$, the integration moves along a $\Gamma \approx 1$ curve, forcing the density to remain low and almost constant over a large radial extent. Since enough column mass (or equivalently optical depth) still has to be accumulated in order to meet the lower boundary condition, the only way the star can react is by expanding in radius (see also discussion in Owocki 2014). Comparing this now to our dynamic solutions shows that, for the same $\Gamma_e$, inclusion of the dynamical terms reduces the inflation somewhat. Nonetheless, $R_{ph}$ still lies very far away from the core in such outflow models of dynamically inflated envelopes; indeed, for our standard $\Gamma_e = 0.40$ we obtain $R_{ph} = 4.48R_\odot$ and $T_{\text{ph, eff}} \approx 62$ K. Such a close agreement of photospheric radii in dynamic and static models is however not generally found. Namely, a very small increase to $\Gamma_e = 0.41$ in the static model leads to an order of magnitude increase of the star’s photospheric radius (see Fig. 4), in contrast to the dynamic model where this barely affects the location of $R_{ph}$.

The analysis above assumes that all luminosity is carried by radiation. In stellar models, the strong increase in opacity around the iron bump will typically lead to an onset of convection, such that $L = L_{\text{rad}} + L_{\text{conv}}$. In principle, this may alleviate the inflation by allowing a portion of the luminosity to be carried by convection, lowering the effective $\Gamma_e \sim L_{\text{rad}}$. However, for the conditions prevailing in WR stars convection in these near-surface layers should be very inefficient. Following Gräfener et al. (2012), an upper limit to the fraction of the total stellar flux $F$ that can be carried by convection is:

$$F_{\text{conv}} \frac{\Gamma_e}{F} = 0.0034 \frac{10^5 \text{ K}}{T_{\text{c, eff}}}. \quad (25)$$

This means that for the $T_{\text{c, eff}} > 10^5$ K considered in this paper, less than a percent of the total luminosity will be carried by convection.

This convective inefficiency is confirmed by the computation of WR stars using the stellar structure and evolution code package MESA (Paxton et al. 2019). Namely, using the standard mixing-length theory (MLT) prescription for convection shows that such stellar structure and evolution computations indeed undergo similar inflation in the WR stage as seen here in Fig. 4. However, in these stellar evolution simulations envelope inflation and the associated density inversions often imply prohibitively short time steps within the model calculations. To prevent this from happening, such stellar models often invoke an additional energy transport that is far greater than that implied by the upper-limit estimate of $L_{\text{conv}}$ above (see, for example, the so-called MLT++ prescription in MESA, Sect. 7.2 in Paxton et al. 2013). This then forces $L_{\text{rad}}$ to always be low enough such that the calculation can proceed.

To mimic these tricks, in the next step we artificially reduce $\Gamma_e \sim L_{\text{rad}}$ by introducing $L = L_{\text{conv}} + L_{\text{rad}}$. Then using $L_{\text{rad}}$ in Eq. (20), while computing the radiation pressure from the total luminosity in Eq. (21), we solve the differential equations exactly as above. By then assuming different ratios $L/L_{\text{rad}}$ for the same fixed total luminosity, we can directly compare dynamic and static inflation models with and without such a reduction in radiative luminosity. Analogous to the left panel, the right panel of Fig. 4 shows the radial density structure of a case with reduced radiative luminosity $L/L_{\text{rad}} = 4$ (solid line), comparing this to...

---

5 For the fixed stellar mass and electron scattering mass absorption coefficient the variation of $\Gamma_e$ is equivalent to the variation of $L_{\text{rad}}$.

6 Detailed description of these models as well as Input files to reproduce our MESA simulations are provided at https://doi.org/10.5281/zenodo.4054811
the original case $L/L_{\text{rad}} = 1$ (solid, marked line). The ratio of $L/L_{\text{rad}} = 4$ here is chosen such that the stellar envelope no longer experiences a density inversion. The figure demonstrates clearly that the two solutions have vastly different radial scales; while the original model had $R_{\text{ph}} = 4.7 R_\odot$ and $T_{\text{eff}} = 56$ K, the model with reduced radiative luminosity has a very hot $T_{\text{eff}} = 121$ K and a photospheric radius that lies less than a percent above the core $R_c = R_\odot$.

The reason for these drastically different stellar photospheric radii is the same as described earlier; including an additional (artificial) energy transport reduces the effective $\Gamma_r \sim L_{\text{rad}}$, so that a dense exponential atmosphere with small scale height is formed. This then avoids inflation and density inversions, and the upshot is a hot and compact WR stellar surface. This is a good example of how envelope inflation and density inversions are naturally develop a dynamically inflated outflow region.

4. Time-dependent numerical hydrodynamic simulations

The previous section presented calculations in the steady-state limit, using various degrees of approximations for solving the dynamical (and static) equations. Building on the same basic formalism, this section now presents full time-dependent numerical hydrodynamics simulations for spherically symmetric WR wind outflows. A key objective is to examine whether such time-dependent simulations relax to similar solutions as the simplified steady models of Sect. 3.

The hydrodynamic simulations are performed using the finite volume code MPI-AMRVAC (Xia et al. 2018) to solve Eqs. (1), (4), and (7). We use the HLL solver (Harten 1983) with a MUSCL flux limiter (van Leer 1979). The radiative acceleration is computed as in Sect. 3.3 by summing up the contributions from OPAL and CAKE-like opacities, $\Gamma_{\text{tot}} = \Gamma_{\text{OPAL}} + \Gamma_{\text{CAKE}}$. Here the OPAL contribution is trivially obtained from the local density and temperature, and the CAKE contribution from a simple central finite difference scheme applied to Eq. (18). To avoid information propagating over multiple cells in a single integration we further limit the integration time step $\Delta t$ by:

$$\Delta t = \min \left( \frac{d_{\text{CFL}}}{2}, \frac{0.3 \sqrt{\Delta r}}{g + g_f} \right),$$

where $d_{\text{CFL}}$ is the time step set by the standard Courant-Friedrichs-Lewy condition (Courant et al. 1928), and $\Delta r$ the width of one numerical cell.

As Eq. (7) is not the standard way of computing the energy balance in MPI-AMRVAC we have implemented an additional routine to handle this. In this subroutine the optical depth Eq. (8) is first computed by trapezoid integration starting from the outer boundary $i = i_{\text{max}}$ setting $\tau(i_{\text{max}}) = \tau_{\text{out}}$ as before, inwards to $i = i_{\text{min}}$. The radial temperature structure $T_i$ is then updated at each hydrodynamical time step according to Eq. (7). For simplicity, we here define $R_c$ to always be at the lower boundary of the simulation.

**Fig. 5.** Surface plot of velocity as a function of time and reduced radius $r$ for the model as described in text. The figure demonstrates how the velocity profile relaxes from the initially assumed $v_p$ to (quasi) steady-state profile over $\approx 40$ ks.

4.1. Initial and boundary conditions

Analogous to our steady-state simulations, we define the outer boundary to be located at some radius $R_{\text{max}}$, and use the same optical depth and temperature conditions as described in the previous section, Eq. (7) and the pre-specified minimum temperature (see above). As in, for instance, Driessen et al. (2019), the numerical outer boundary conditions on the velocity and density are set by simple extrapolation from the outer most points of the simulation grid. To properly resolve the sonic point we set the inner boundary to a lower radius than the expected sonic point $R_s$, i.e. now $R_{\text{min}} \equiv R_s = 0.99 R_c < R_s$. At this $R_{\text{min}}$ we then fix the lower boundary density $\rho_s$ and allow the velocity to adjust to the overlying wind conditions (see, e.g. Owocki et al. 1988). $\rho_s$ is initially estimated from our corresponding steady-state models by simply assuming hydrostatic equilibrium below the sonic point. The stellar mass and luminosity are still as in Table 1.

The initial wind condition is an analytic outflow structure, in the form of a simple $\beta$-law:

$$v_p = v_\infty \left( 1 - \frac{R_c}{r} \right)^{\beta},$$

where the terminal velocity $v_\infty = 2 M_*/(\Gamma - 1)/R_\odot$, and $\beta = 0.5$ are derived from a simple assumed $\Gamma = \text{const} > 1$. The parameter $b$ sets the minimum initial velocity $v_{\text{min}}$ at $r = R_c$, here chosen such that $v_{\text{min}} \approx 50$ km s$^{-1}$. The equation of continuity then directly provides the initial density structure. Finally, the initial temperature structure is computed from Eq. (7) with the opacity set according to the assumed input $\Gamma$ from above. Using these initial and boundary conditions, numerical time integration is carried out until the wind relaxes to a (quasi) steady state. We, however, note that the results of our simulations are not sensitive to these assumed initial conditions.

4.2. Time-dependent dynamic inflation model

Starting from the initially assumed structure the wind outflow gradually relaxes to a hydrodynamically consistent structure. The velocity relaxation is displayed in Fig. 5 as a surface plot, where along one horizontal axis the physical time $t$ in ks of the simulation is shown and along the other the radius in $x = 1 - R_c/r$. The vertical axis then measures velocity (in km s$^{-1}$). At $t = 0$ the
initial velocity structure, \(\alpha_0\), is visible, however as time increases this \(\beta\)-type structure gradually evolves towards the three-phased velocity profile discussed in Sect. 3.5. Around at \(t \approx 40\) ks the simulation has relaxed to a state very similar to that found in our corresponding steady-state model (Sect. 3.5).

Running the simulation for in total 600 ks, Figs. 6a and b show the Eddington ratio \(\Gamma\) and the velocity profile of the final time step. From Fig. 6a we observe that, just as in the steady-state model, the CAK-like force near the lower boundary on average only has a small contribution to the total force; contrarily, near the outer boundary, it is dominant. The radiation force from the OPAL contribution has the opposite behaviour, dominating at the outer parts. This then again leads to a velocity profile (solid line in Fig. 6b) with a non-monotonic behaviour, which clearly can not be fit with the simple \(\beta\)-type velocity law assumed in the initial conditions (dotted line).

This velocity profile can be directly compared to that found in our corresponding steady-state model, illustrated by the dashed line in Fig. 6b, which shows close agreement between the two. The mass loss of the time-dependent model is \(M = 1.64 \times 10^{-5} M_\odot\,\text{yr}^{-1}\), which also agrees well with the mass-loss rate of \(M = 1.47 \times 10^{-5} M_\odot\,\text{yr}^{-1}\) from our steady-state model (see Sect. 3). In this way, our time-dependent models demonstrate that the dynamically inflated solution discussed in the previous section indeed works as a stable attractor for the stellar wind envelope, confirming our basic conclusions regarding a wind outflow controlled primarily by OPAL opacities in the inner regions, and by the CAK-like force in the outer. The small differences in velocity magnitude and mass loss between steady-state and time-dependent models are mainly related to differences in setting the lower boundary. In steady-state computations we define the sonic point to be exactly at the lower boundary, whereas in time-dependent computations it is allowed to self adjust so that the sub-sonic part is also resolved.

### 4.3. \(M\) dependency on CAK \(\alpha\)

A general finding of our baseline simulations in Sects. 3 and 4 is that (as long as the wind can escape), the mass-loss rate is primarily controlled by the conditions in the lower wind; in contrast, the terminal wind speed is controlled mainly by the outer wind conditions. Moreover, while it has turned out that a steady-state model, such as the one presented in Sect. 3, is quite difficult to converge, the time-dependent simulations of this section are computationally somewhat easier to handle.

Therefore, we have used our time-dependent set-up to further explore the impact of the CAK-like force parameters on the predictions of \(M\) and \(v_\infty\). We investigate the impact of these parameters by varying only \(\alpha_{\text{min}}\) and \(\alpha_{\text{max}}\), however we point out that comparable effects could also be achieved by instead introducing corresponding radial variations of the second line-force parameter \(\tilde{Q}\). To this end, we test a range of values \(\alpha_{\text{max}} \in [0.60, 0.66]\) and \(\alpha_{\text{min}} \in [0.48, 0.53]\), corresponding roughly to the scatter of \(\alpha\) observed in the MC simulations displayed in Fig. 2. The results of these tests are summarised in Tables 3 and 4, along with the mass-loss rates and terminal velocities found for the different model runs. In addition, we also tested variations in the spatial position of the \(\alpha_{\text{max}}\) to \(\alpha_{\text{min}}\) transition for the standard CAK force parameters in the range \(x \in [0.3, 0.7]\). However, for these tests, no significant influence on the mass-loss rates of the models have been observed. Therefore, the following subsections focus exclusively on varying the values of \(\alpha_{\text{max}}\) and \(\alpha_{\text{min}}\).

### Table 3. Summary of mass-loss rates and terminal wind speeds for models with different values of \(\alpha_{\text{min}}\).

<table>
<thead>
<tr>
<th>(\alpha_{\text{min}})</th>
<th>(\alpha_{\text{max}})</th>
<th>(M/10^{-5})</th>
<th>(M_{\text{CAK}}/10^{-5})</th>
<th>(v_\infty)</th>
</tr>
</thead>
<tbody>
<tr>
<td>0.48</td>
<td>1.59</td>
<td>4.60</td>
<td>2765</td>
<td></td>
</tr>
<tr>
<td>0.50</td>
<td>1.64</td>
<td>2.70</td>
<td>2063</td>
<td></td>
</tr>
<tr>
<td>0.52</td>
<td>1.68</td>
<td>1.66</td>
<td>1279</td>
<td></td>
</tr>
<tr>
<td>0.53</td>
<td>--</td>
<td>1.33</td>
<td>--</td>
<td></td>
</tr>
</tbody>
</table>

**Notes.** The columns provide \(\alpha_{\text{min}}\) (value of \(\alpha\) parameter at the outer boundary), \(\alpha_{\text{max}}\) (value of \(\alpha\) parameter at the inner boundary), the mass-loss rate of the model \(M/10^{-5}\) in \(M_\odot\,\text{yr}^{-1}\), the CAK mass loss \(M_{\text{CAK}}/10^{-5}\) in \(M_\odot\,\text{yr}^{-1}\) corresponding to \(\alpha_{\text{min}}\), and the terminal velocity \(v_\infty\) in \(\text{km s}^{-1}\). The model with \(\alpha_{\text{min}} = 0.53\) failed to provide sufficient force to drive the outflow to the outer boundary, leading to termination of the numerical simulation (see text).
Table 4. Summary of mass-loss rates and terminal wind speeds for different values of \( \alpha_{\text{max}} \).

<table>
<thead>
<tr>
<th>( \alpha_{\text{min}} )</th>
<th>( \alpha_{\text{max}} )</th>
<th>( M/10^{-5} ) ( (M_\odot \text{yr}^{-1}) )</th>
<th>( \dot{v}_{\infty} ) ( (\text{km s}^{-1}) )</th>
</tr>
</thead>
<tbody>
<tr>
<td>0.60</td>
<td>2.13</td>
<td>1787</td>
<td></td>
</tr>
<tr>
<td>0.63</td>
<td>1.84</td>
<td>1937</td>
<td></td>
</tr>
<tr>
<td>0.66</td>
<td>1.64</td>
<td>2063</td>
<td></td>
</tr>
</tbody>
</table>

Notes. The columns are as in Table 3.

4.3.1. Dependency on \( \alpha_{\text{min}} \)

As \( \Gamma_{\text{CAK}} \) is the prevalent driver in the outer wind, one might initially expect a similar dependence of the mass-loss rate on \( \alpha_{\text{min}} \) as given by the standard CAK model. The CAK expression for the mass-loss rate \( M_{\text{CAK}} \)-typically derived from critical-point analyses for \( \Gamma_{\text{tot}} = \Gamma_0 + \Gamma_{\text{CAK}} \) in the radial streaming limit, is:

\[
M_{\text{CAK}} = \frac{L}{c^3} \frac{\alpha}{1 - \alpha} \left( \frac{Q_{\text{e}}}{1 - \Gamma_{\text{e}}} \right)^{\frac{5}{2}}.
\]

(27)

From this expression, it directly follows that \( M_{\text{CAK}} \) increases steeply if \( \alpha \) is decreased while keeping all other parameters constant. However, it can be seen from Table 3 that in our models \( M \) varies only marginally across the range of considered \( \alpha_{\text{min}} \) values. This distinguishes these optically thick WR simulations from standard CAK-type models applied to the optically thin winds of O-type stars. We further confirm the finding from the steady models that if \( \alpha_{\text{min}} \) is increased too much, the line force becomes insufficient to sustain the outflow. This happens because the line acceleration in the outer wind must be sufficient to prevent fallback of the mass loss initiated at the Fe-opacity bump. That is, the line acceleration must provide enough additional energy such that the previously introduced \( \mathcal{W} \geq 0 \) condition is fulfilled. As alluded to above, the CAK mass-loss rate formula cannot be directly used to predict the mass-loss rate equals that of our actual model. For the given model with \( \alpha_{\text{min}} = 0.62 \), \( \Gamma_{\text{CAK}} = 0.14 \), and for the \( \alpha_{\text{max}} = 0.66 \) we find \( \Gamma = 0.02 \), which is much lower even than our initial order of magnitude estimate \( \Gamma \approx 0.1 \) in Sect. 3.4. This further supports that the CAK force has a negligible contribution at the sonic point. Moreover, since those inner parts accumulate the majority of the integrated wind optical depth, they also primarily control the lower-boundary temperature to which the overlying wind adjusts, and thereby also the mass-loss rate.

5. Discussion

5.1. Implication for core radius problem

The dynamic models presented in Sects. 3 and 4 provide a natural explanation to the so-called core radius problem of classical WR stars (see Sect. 1). To understand this, we introduce the standard Rosseland mean optical depth scale

\[
\tau_{\text{Ros}} = \int_{r}^{\infty} \kappa_{\text{Ros}} \rho \, dr = \int_{r}^{\infty} \kappa_{\text{OPAL}} \rho \, dr,
\]

(28)

where \( \kappa_{\text{Ros}} \) is computed using the Rosseland mean opacities from the OPAL tabulation, such that \( \kappa_{\text{Ros}} = \kappa_{\text{OPAL}} \) throughout this work.

Then, following the standard spectroscopic model approach of fitting an assumed \( \dot{v}_{\infty} \) velocity profile to the entire supersonic region, Fig. 7 directly illustrates how the hydrostatic core \( R_{c}^{\text{op}} \) (where \( \dot{v}_{\infty} \) reaches sub-sonic velocities) in that case would be located at a radius \( R_{c}^{\text{op}} > R_{c} \). Indeed, the core radius recovered in this way is a factor \( \approx 2.6 \) times larger than the true value, demonstrating the basic challenge of determining WR hydrostatic radii from spectroscopic data (e.g. Crowther 2007). The discrepancy essentially stems from the fact that \( \tau_{\text{Ros}} = 2/3 \) is reached already at very high radii (see the grey area in Fig. 7), so that only the outermost velocity law is visible to us. Observational estimates of the hydrostatic stellar core radius must thus be obtained by some extrapolation of the velocity law assumed in the spectroscopic model, without any knowledge of the true velocity field in the invisible inner regions.

The dynamic models presented in this paper explain this long-standing discrepancy simply by their extended (dynamically inflated) region of low-velocity outflowing material above the hydrostatic stellar core.

To further illustrate this effect, let us inspect the observational positioning of classical WR stars on the Hertzsprung–Russell diagram (HRD), where the stars are placed according to their observationally inferred luminosities and hydrostatic core effective temperatures. Figure 8 here shows the HRD where

Sander & Vink (2020), who find a correlation between \( M \) and \( \dot{v}_{\infty} \). We further discuss possible reasons for this in Sect. 5.4.

4.3.2. Dependency on \( \alpha_{\text{max}} \)

In contrast to \( \alpha_{\text{min}} \), \( \alpha_{\text{max}} \) has little to no effect on determining the terminal velocity of the outflow. Nevertheless, it can affect \( M \). This is illustrated in Table 4, where a modest increase in \( \alpha_{\text{max}} \) is found for decreasing values of \( \alpha_{\text{max}} \). We note, however, that again the magnitude of the mass loss variation is small in comparison to that seen in CAK-type wind models of optically thin O-stars.

This rather weak dependence on the CAK force stems from the fact that the dominant contribution to the total radiation force comes from the OPAL opacities in the regions near the stellar core (see also Sect. 3). At the sonic point for \( \alpha_{\text{max}} = 0.6 \), we find \( \Gamma_{\text{CAK}} = 0.14 \) and for the \( \alpha_{\text{max}} = 0.66 \) we find \( \Gamma = 0.02 \), which is much lower even than our initial order of magnitude estimate \( \Gamma \approx 0.1 \) in Sect. 3.4. This further supports that the CAK force has a negligible contribution at the sonic point. Moreover, since those inner parts accumulate the majority of the integrated wind optical depth, they also primarily control the lower-boundary temperature to which the overlying wind adjusts, and thereby also the mass-loss rate.
the observed galactic sample of WR stars by Hamann et al. (2019) and Sander et al. (2019) is placed. Positions of these stars on the HRD can then be compared to the location of the so-called helium zero age main sequence (He-ZAMS; dashed line in figure), computed here with MESA using the standard mixing-length theory for convection with solar metallicity and relative metal fractions as given by Asplund et al. (2009). On average, observationally inferred positions of WR stars are then expected to lay to the left of this He-ZAMS line. This is because typical stellar evolution models, where an additional energy transport is typically also invoked in order to prevent the WR cores from inflating (see Sect. 3.5), occupy the region to the hotter side of He-ZAMS on the HRD. Figure 8, however, shows that the average position of these WR stars (indicated by + in the figure) is located on the cooler side of the He-ZAMS instead. To improve the agreement between spectroscopy and evolution predictions a simple correction factor ≈3 can be applied to the spectroscopic radii, which then shifts the core effective temperature location (now identified on Fig. 8 by x). And indeed, such a correction factor matches quite well with the correction factor implied by our dynamic inflation models above.

5.2. Empirical constraints and model dependencies of mass loss and terminal velocity

The basic model presented in the previous sections shows an overall quite good agreement with empirical constraints on terminal velocities and mass-loss rates of WR stars. Figure 9 plots such empirically inferred values of $M$ and $v_\infty$, again from Hamann et al. (2019) and Sander et al. (2019). Compared to the mass-loss rates and terminal velocities predicted by our hydrodynamic and steady-state models (summarised in Table 5), the latter is located at the high end of the inferred values. However, since $v_\infty$ is primarily determined by the line force in the outer wind regions, which here is parametrised by the simple radial streaming CAK-approximation outlined in previous sections, a more detailed approach will be necessary to make more quantitative comparisons to empirical $v_\infty$. Inspection of Fig. 9 also reveals that the empirical mass-loss rates and terminal wind speeds show no prominent anti-correlation. This further supports another basic characteristic of our models, namely that $M$ and $v_\infty$ are quite decoupled (see Sect. 4.3.1).

Table 5. Summary of derived parameters of our steady-state and time-dependent models.

<table>
<thead>
<tr>
<th>Model</th>
<th>$M$ ($M_\odot$ yr$^{-1}$)</th>
<th>$v_\infty$ (km s$^{-1}$)</th>
<th>$R_{\text{ph}}$ ($R_\odot$)</th>
<th>$T_{\text{ph, eff}}$ (kK)</th>
</tr>
</thead>
<tbody>
<tr>
<td>Steady-state</td>
<td>$1.47 \times 10^{-5}$</td>
<td>2200</td>
<td>4.48</td>
<td>62</td>
</tr>
<tr>
<td>Time-dependent</td>
<td>$1.64 \times 10^{-5}$</td>
<td>2063</td>
<td>4.64</td>
<td>60</td>
</tr>
</tbody>
</table>

Notes. Listed are mass-loss rate, terminal velocity, radius of photosphere, and effective temperature at photosphere.
5.3. Dependence on metallicity

The model of dynamic inflation presented in this paper relies on the fact that the \( \Gamma = 1 \) condition is reached already at the Fe-opacity bump. As such it is sensitive to the variation of opacity at the Fe-opacity bump, which is directly controlled by metallicity (e.g. Cantiello et al. 2009). Qualitatively, the model of dynamic inflation should respond to a decrease or increase in metallicity by reducing or enlarging the scale of inflation and the associated mass loss. Moreover, at low enough metallicity the \( \Gamma = 1 \) condition will not be fulfilled at the Fe bump, in which case dynamic inflation will no longer take place from the hot Fe bump, and a standard optically thin wind develops instead. This behaviour is also in line with the recently published models by Sander & Vink (2020).

5.4. Comparison to co-moving frame models

As mentioned above, recently Sander et al. (2020) and Sander & Vink (2020) published time-independent wind simulations of classical WR stars. These models solve the same steady-state e.o.m. as here\(^8\), however using a different method to calculate the radiative acceleration. There \( \Gamma(r) \) is derived from full solutions of the frequency-dependent radiative transfer equation in the co-moving frame (CMF), without the use of any parameterisation to estimate the line-force contribution (see also Sundqvist et al. 2019; Björklund et al. 2021, for similar approaches applied to O-stars). Although these models thus compute \( \Gamma(r) \) for a given velocity and density structure in a more detailed way than here, this CMF method (as currently implemented) has one major disadvantage. Because of the way the CMF transfer equation is numerically solved, it can only be applied to monotonically increasing (or decreasing) velocity fields \( \nu(r) \). As such, this method cannot be used to derive \( \Gamma(r) \) for the type of non-monotonic velocity structures found here (see Figs. 3b, 6b).

The way Sander et al. (2020) overcome this issue is by assuming an ad hoc very high degree of clumping in the WR outflow (see also Gräfener & Hamann 2005). They parameterise this using a simple model where all wind mass is assumed to be concentrated within overdense clumps, such that the densities of these clumps are \( \rho_{\text{cl}} = \langle \rho \rangle / f_{\text{vol}} = D \rho(r) \), where \( \langle \rho \rangle \) is the mean density (assumed to be preserved with respect to a smooth model), \( f_{\text{vol}} \) the volume fraction of the total wind contained by clumps, and \( D \) the clump-overdensity factor.

By adopting a very high \( D = 50 \) (\( f_{\text{vol}} = 0.02 \)), the ionisation balance of the wind is shifted so that more effective driving lines become available, and the line force is thereby increased enough to avoid any deceleration regions. When assuming instead a more modest \( D = 10 \) in their models, they do experience the same type of \( \Gamma < 1 \) regions as here, which leads then to a non-monotonic \( \nu(r) \) that cannot be handled by the CMF radiative transfer (see Fig. 1 in Sander et al. 2020, and their corresponding discussion). Since observations of electron scattering wings in WR outflows suggest quite modest values \( D \approx 4-10 \) (see overviews by Crowther 2007; Puls et al. 2008), and theoretical wind-clumping models following the line-driven instability (Owocki et al. 1988) have so far only been developed for OB-stars (with again typical values \( D \approx 10 \); Sundqvist et al. 2018; Driessen et al. 2019), it is at present not clear how the high clump densities needed to keep \( \nu(r) \) monotonic in CMF-based WR models might be physically justified.

The models presented here are thus very complementary to such CMF-based simulations. Although our more simplified treatment of \( \Gamma \) involves certain approximations (as discussed in previous sections) it allows us to model regions of stagnation and deceleration (see Sects. 3 and 4), whereas such non-monotonic flows are incompatible with the methods currently used in CMF-based calculations. Moreover, the method presented here allows for time-dependent simulations that otherwise would not be computationally feasible. In this respect, we also recall our finding that if the line force in the outer wind is decreased too much, the wind not only experiences regions of deceleration but may eventually reach zero velocity. In the 1D simulations presented here, this leads to failed wind solutions and model termination. In a multi-dimensional simulation, one may speculate that it might instead result in a very complex wind structure of co-existing regions of upflows and inflows. In turn, this may then cause shocks and perhaps increased levels of clump formation. These could be simulated in multi-dimensional hydrodynamics simulations using the method we present here.

The models presented here also demonstrate that even with multiple extended regions where \( \Gamma < 1 \), the accumulated net energy of the wind can still be positive (i.e., we can still have \( W \geq 0 \)). This suggests that the WR outflow can be driven without invoking such a high degree of clumping, but instead allowing for non-monotonic velocities. For example, let us consider the lower panel of Fig. 1 in Sander et al. (2020), where the authors provide \( \Gamma(r) \) not only for their final \( D = 50 \) model (their solid line) but also for their collapsed \( D = 10 \) solution (their dashed line). From these profiles, we estimated the net energy corresponding to both models and found that, indeed, both of the force configurations provide \( W > 0 \). As such, both solutions may actually escape the stellar potential, but since the \( D = 10 \) model would have contained regions of negative acceleration it could not be treated by the assumed CMF radiative transfer framework.

Note that Sander et al. (2020) make the argument that although the assumed very high degree of clumping influences \( v_{\infty} \) significantly, it does not have a major impact on \( M \), since clumping is assumed to be present only at supersonic velocities. This is quite consistent with our finding here. On the other hand, Sander & Vink (2020) also find a correlation between \( M \) and \( v_{\infty} \), which we do not necessarily observe in our models. This result, however, might simply be related to them forcing a monotonous velocity field in their simulations, since the same correlation was also found in the \( \beta \)-law WR models by Gräfener et al. (2017).

6. Summary and future work

This paper has presented a model for the wind outflows of classical Wolf-Rayet stars, based on a hybrid opacity method where OPAL opacities are used in combination with a CAK-like line force parametrisation. The latter is used here to account for the effects of Doppler shifts upon spectral line opacity in an approximate way. Our hybrid opacity model essentially results in a two stage WR stellar wind: a supersonic outflow is first initiated in optically thick layers (at the so-called Fe bump) by the OPAL opacities. However, these opacities are not able to prevent fallback upon the core, and so it is the CAK-like force that takes over the driving in the outer regions and ensures that the initiated outflow can also escape the stellar potential.

Our approach leads to deep-seated wind initiation with high mass-loss rates and terminal velocities (see Table 5), in the range of values typically inferred for classical WR stars by spectroscopic analyses. The simulations display dense and
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